



## **Mawson Canada Pty Ltd**

Isa South East Geophysics Project

Round 2 Collaborative Exploration Incentive

CEI0034

Final Report

Tenure: EPM 26477, EPM 26479, EPM 26481, EPM 26483

Holder and Operator: Mawson Canada Pty Ltd

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Date of Report: August 2019

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## **1. Executive Summary**

This report summarises exploration activity undertaken by Mawson Canada Pty Ltd (Mawson) as part of the Queensland Government Round 2 Collaborative Exploration Incentive (CEI).

Work included an aeromagnetic survey and a ground gravity survey. These surveys have increased data density in a data-sparse environment. Preliminary visualisation of both data sets indicates they will be of positive value to ongoing exploration.

## **2. Introduction**

Mawson's Isa South East Project represents frontier exploration terrane. The >1300 square km land package is obscured by deep post-Proterozoic cover with only historical drill holes penetrating basement. This is despite the parts of the area being underlain by (i) similar magnetostratigraphy that hosts the world class Cannington silver-lead-zinc mine and (ii) major structural boundaries, including the Cloncurry fault zone and secondary structures which may have acted as conduits for mineralising fluids.

The CEI-cofunded Isa South East Geophysical Project increased the density of existing open file geophysical coverage. This involved closing the line-spacing of the airborne magnetic coverage from 400 m to 200 m. A ground gravity grid was completed at 1km spacing compared to the existing 4 km spacing.

The new magnetic and gravity data sets will permit a refinement of existing lithostructural interpretations and be foundational for subsequent drill targeting.

## **3. Project Location and Access**

The Isa South East Project is centred approximately 150km southeast of Cloncurry and 25km east of South 32's Cannington mine (Figure 1). A network of unsealed station tracks provides excellent access throughout the tenements. Many of these tracks were investigated as part of ground reconnaissance activities in July 2019.

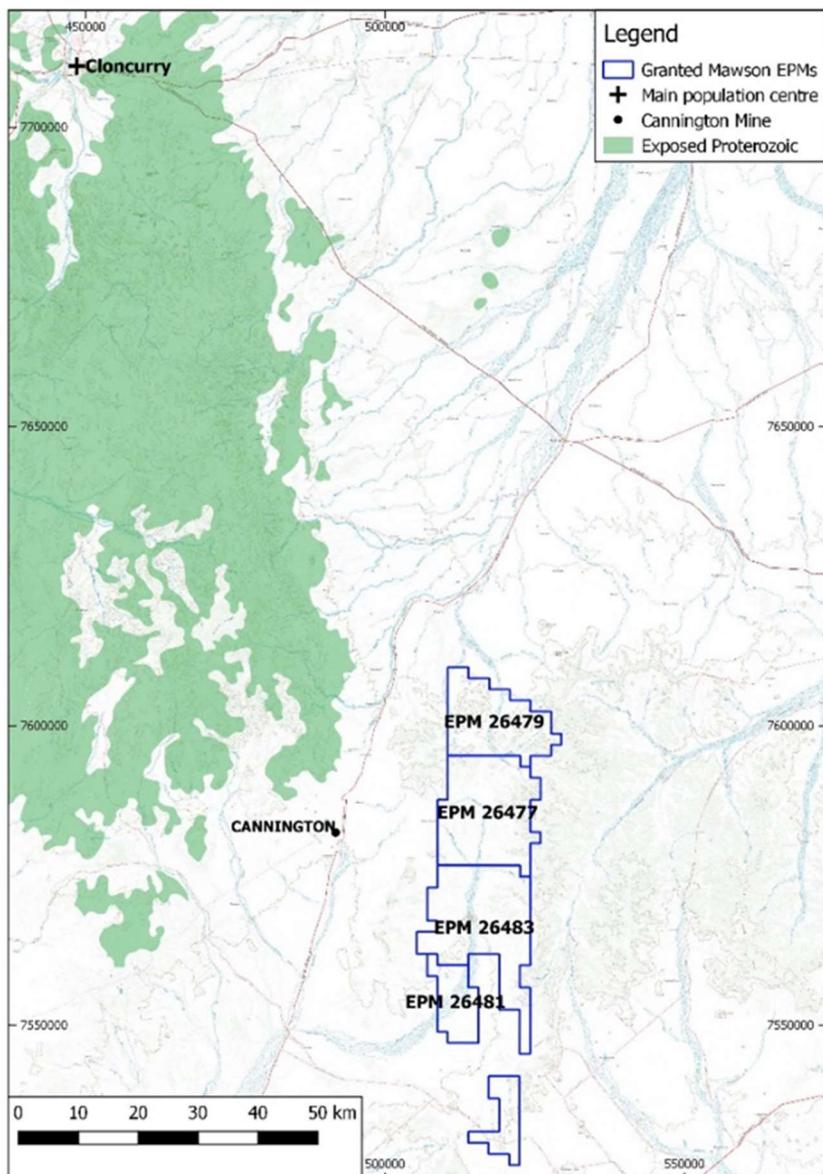


Figure 1. Location map of Mawson's Isa South East project. EPM26481 is two non-contiguous blocks.

#### 4. Regional Geology

Throughout the project area Proterozoic basement is obscured by a thick package of Mesozoic sediments (Eromanga Basin sequence). Depth of cover, based on limited basement drilling and information from water bores, ranges from 250 m to 400 m. Exploration is therefore driven by magnetic and gravity geophysical methods with a commitment to drilling targets generated. As the cover is conductive, electromagnetic methods are unlikely to be effective in generating anomalies in the Proterozoic basement.

A recent lithostructural interpretation by Hinman (2018) provides an excellent geological context under cover (Figure 2). The interpretation is based on detailed proprietary magnetics and drill hole databases provided by South 32, Minotaur and Sandfire, as well as open file magnetics. While the raw data remains confidential, the interpretation is open file.

The project area and surrounds are interpreted to be dominated by Mount Norna Quartzite and overlying Toole Creek Volcanics, both within the Soldiers Cap Group. Mount Norna Quartzite is significant as it is the host sequence for Cannington. As an indicator of prospectivity, the project area contains ~35 km of strike of Mt Norna quartzite based on the Hinman (2018) interpretation.

The structural grain of the area is north-northwest characterised by tight folding (interpreted as D2). Intruding the sediments are Williams Suite intrusives, of which the thermal aureoles may be important drivers for IOCG mineralisation. The north-northwest trending Cannington Fault Zone is a major boundary, interpreted by some workers to be an original basin-bounding structure (e.g. Spampinato et al. 2015). Multiple thrusts cut the volcanosedimentary package. An array of northwest-trending late faults cut all earlier structures and fabrics.

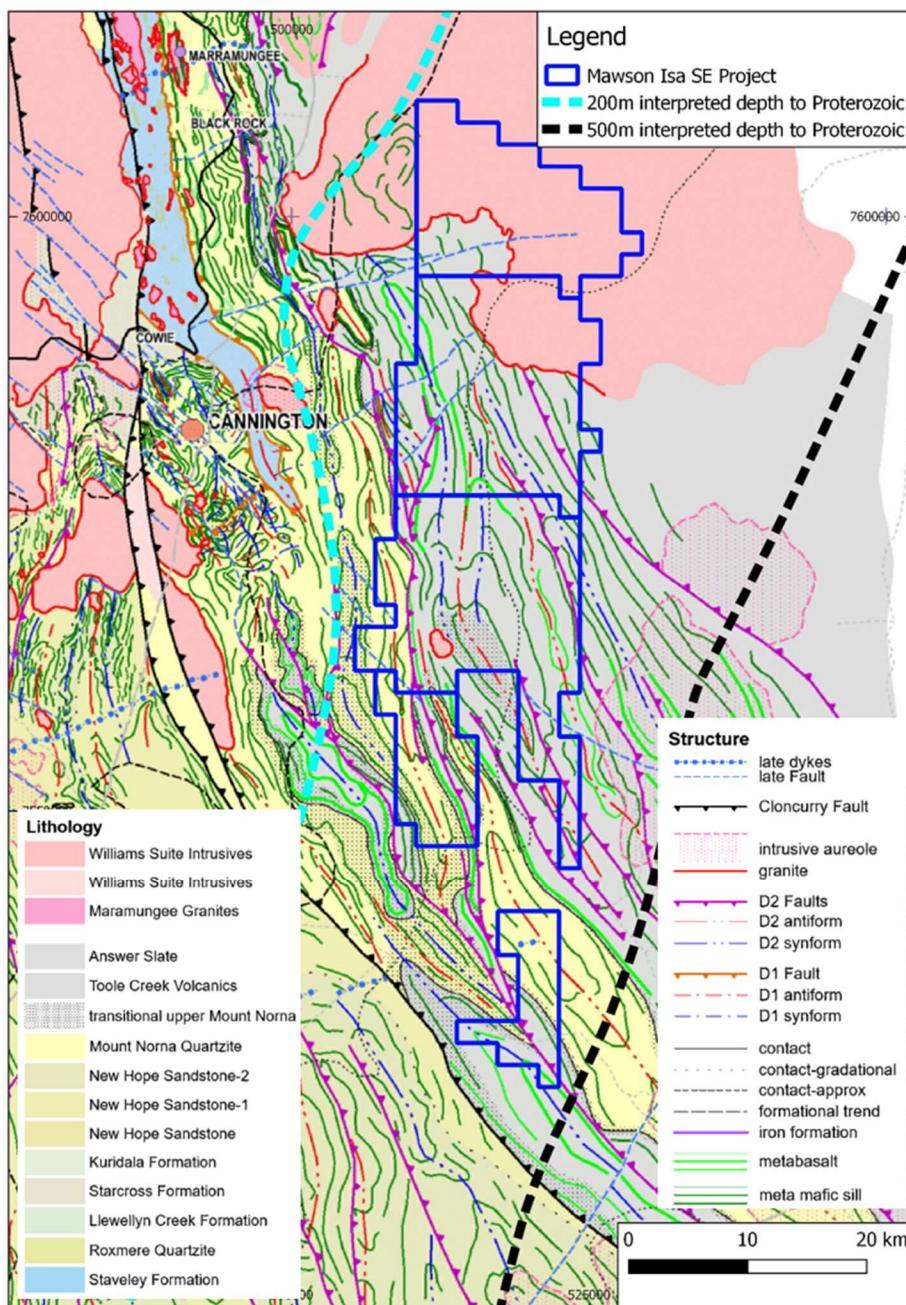


Figure 2. Current lithostructural interpretation of project area and surrounds (modified from Hinman, 2018)

## **5. Previous Exploration**

The Mt Isa area contains a large number of mineral occurrences and world class mines. Most of these discoveries were made within the outcrop and subcrop areas. These areas continue under 100-500 metres of cover particularly to the north, east and south of the Mt Isa mineralized block. Mawson's strategy has been to acquire prospective undercover areas within prospective host sequences in data-poor environments.

In the late 1980s and early 1990s, widespread use of geophysical techniques and drilling persistence led to the discovery of a number of major deposits under cover in the Mt Isa terrain, such as Cannington (about 60 m deep), Century (40 m) and the iron oxide-copper-gold type Ernest Henry deposit (40 m). Since that time grassroots exploration worldwide has decreased, while the search space depth, driven by technology, has increased.

Following the discovery of Cannington in 1990 the area immediately west of Mawson's project area was subject to multiple drilling campaigns (Figure 3), as well as ground and airborne geophysical surveys. However, drilling is completely sparse where cover depths are greater than 200m and the project area remains almost completely unexplored.

Mawson's compilation of previous drilling from open file databases and QDEX company reports indicates only two basement drill holes have been drilled. Both holes were drilled by BHP in 2002. Despite these holes being on current Mawson tenure their details remain confidential under a group reporting technicality.

FALCON airborne gravity gradiometry was flown over the western third of the tenements for BHP in 2001 (Figure 3). However, these data and resultant imagery are considered poor quality given the FALCON technology was at an early stage of development at that time. There are no open file records of any ground geophysical surveys being conducted on current Mawson tenure. Magnetic data collected at the same time as FALCON gravity was on 200 metre line spacing on north-south flight lines (not optimally aligned to the north-northwest geological trend).

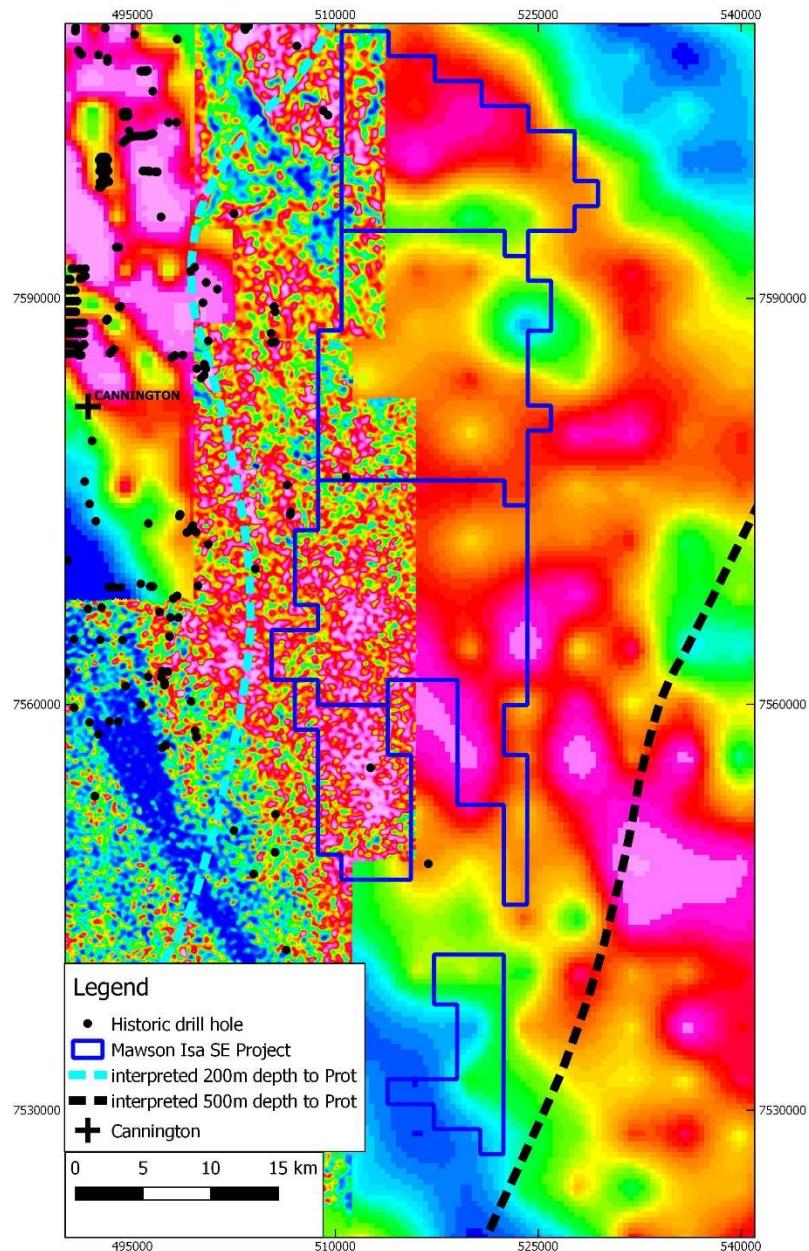


Figure 3. Previous exploration in and west of the project highlighting the lack of drilling in the project – only 2 basement drill holes. Background image covering western half of project is Falcon airborne gravity gradiometry (AGG GDD image approximating 1VD). Elsewhere the background image is Bouguer gravity 1VD as derived from the Geoscience Australia grid (4 km spacing in project area).

With the project EPMs being granted in mid-2018, Mawson has not completed any on-ground exploration work to date. Work has been limited to reprocessing of open file aeromagnetics and ground gravity, plus detailed compilation of historical drilling data.

## 6. Target Characteristics

Mawson's exploration premise is, despite the cover thickness, most deposits will have a detectable geophysical signature. This will be expressed by variable magnetic responses and positive gravity responses. Recent work by the CSIRO (Austin et al. 2016) summarises the magnetic-gravity properties of a range of known Cloncurry orebodies and prospects (Figure 4). While variations in host rock properties will exist at the deposit scale, most

mineralised bodies will be expressed as a gravity high compared to the host rock sequence. This relationship exists regardless of deposit or magnetic style (e.g. Maronan BHT-like vs IOCGs such as Ernest Henry and Osborne).

Mineralisation at the Cannington deposit, which is not included on Figure 4, exhibits a high correlation with magnetic susceptibility and density (Witherly and Mackee, 2015).

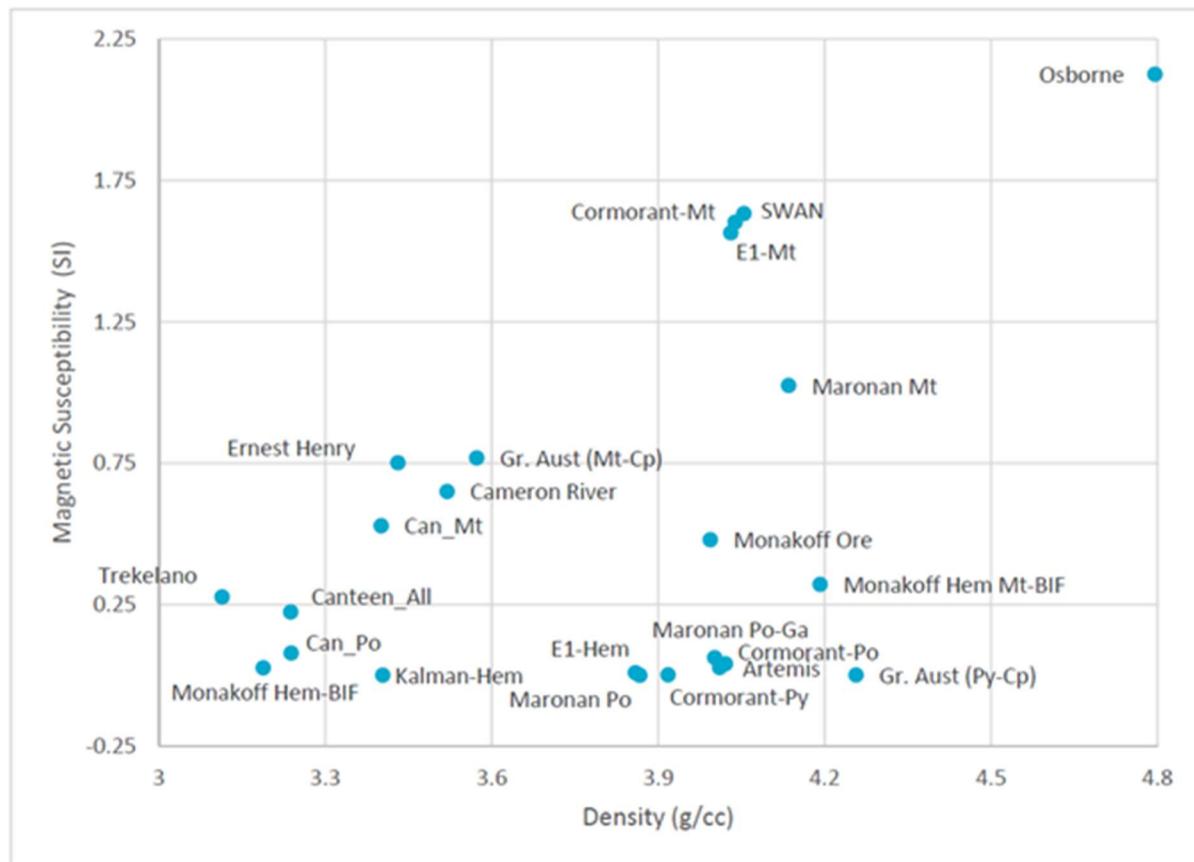


Figure 4. Plot of magnetic susceptibility vs density for ore samples from deposits/prospects assessed in the Cloncurry Uncover 2016 study (Austin et al. 2016).

## 7. Isa South East Geophysics Project - CEI0034

Mawson was successful in qualifying for partial funding under Round 2 of the Collaborative Exploration Incentive (CEI).

Having completed all project activity prior the Project Milestone 1 date (9 August 2019), Mawson is eligible for receipt of \$100,000 representing 75% of direct activity costs.

The project consisted of two geophysical programs:

- Aeromagnetic survey at 200 m line-spacing. This was originally proposed at 100 m line-spacing, but after discussion with our geophysicist, was increased to 200 m. This spacing was considered adequate in light of the minimum 250 m cover thickness.
- Ground gravity survey at 1 km grid-spacing. Infill surveying may be undertaken at a later stage, following interpretation of the combined magnetic and gravity data sets.

## **8. Methods**

### **Aeromagnetics**

The aeromagnetic survey was undertaken by Thomson Aviation Pty Ltd using a Cessna C210 aircraft. The survey was completed from 13 April to 22 April 2019. In addition to the 4 EPMs part of the CEI, the survey also included 3 contiguous Mawson EPMs not part of the CEI grant.

For the CEI tenements only, a total of 4750 line-km was flown.

Survey specifications were:

- Traverse line direction: 090-270 degrees
- Traverse line spacing: 200 m
- Tie-line spacing: 2000 m
- Mean terrain clearance: 40 m

Further detail is contained in Thomson's operations report (Appendix 1), including descriptions of the magnetometer and data acquisition system.

### **Ground gravity**

The ground gravity survey was completed by Haines Surveys from 17 June to 30 June 2019. A helicopter was used to efficiently manoeuvre between the stations. Like the aeromagnetic survey, the ground gravity survey spanned 3 contiguous Mawson EPMs not part of the CEI grant.

For the CEI EPMs only, there were a total of 936 stations.

Details of the survey instrumentation and methodology are contained in the Haines Logistical Report (Appendix 2), including information on survey and gravity control.

## **9. Results and Preliminary Interpretation**

### **Aeromagnetics**

Preliminary processing was undertaken by Robert Smith of Greenfields Geophysics, including RTP (Figures 5 and 6) and first vertical derivative of RTP (Figures 7 and 8).

For each pair of images the left-hand side shows the preexisting magnetic data, mainly 400 m line-spacing and as processed by consultants PGN Geoscience. The right-hand side shows the newly collected data for comparison. All images are rendered using a linear scale from -400 to +500 nT.

Immediately apparent in the new data is the increased resolution of north-northwest trending magnetostratigraphy, fold closures and truncating faults. Isolated magnetic highs are better resolved and some of these may be non-stratigraphic and require follow-up assessment (Figure 5).

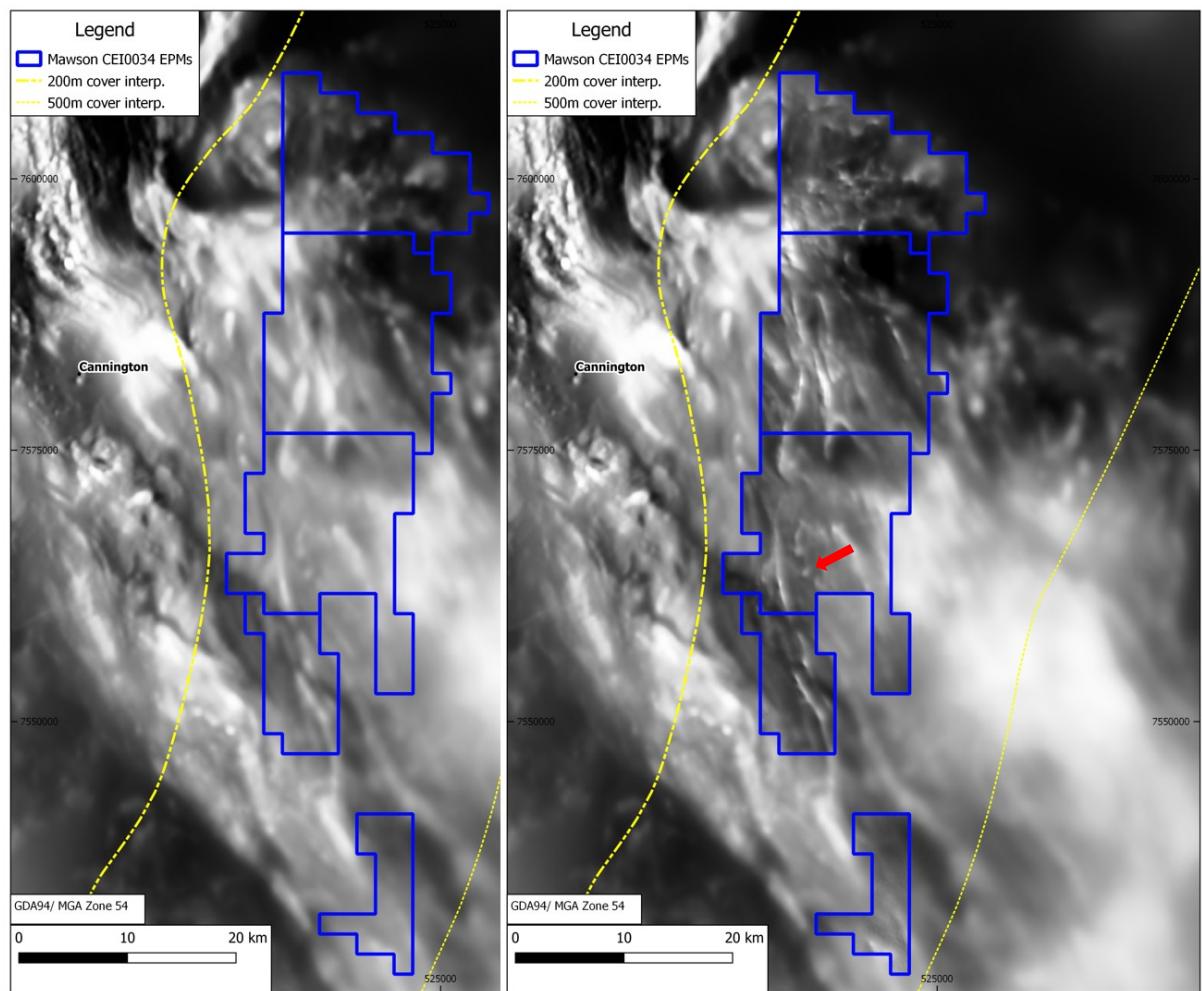


Figure 5. RTP greyscale magnetics. LHS = existing open file data, mainly 400m line-spaced. RHS shows newly collected data within CEI EPMs. Red arrow points to possible non-stratigraphic magnetic high.

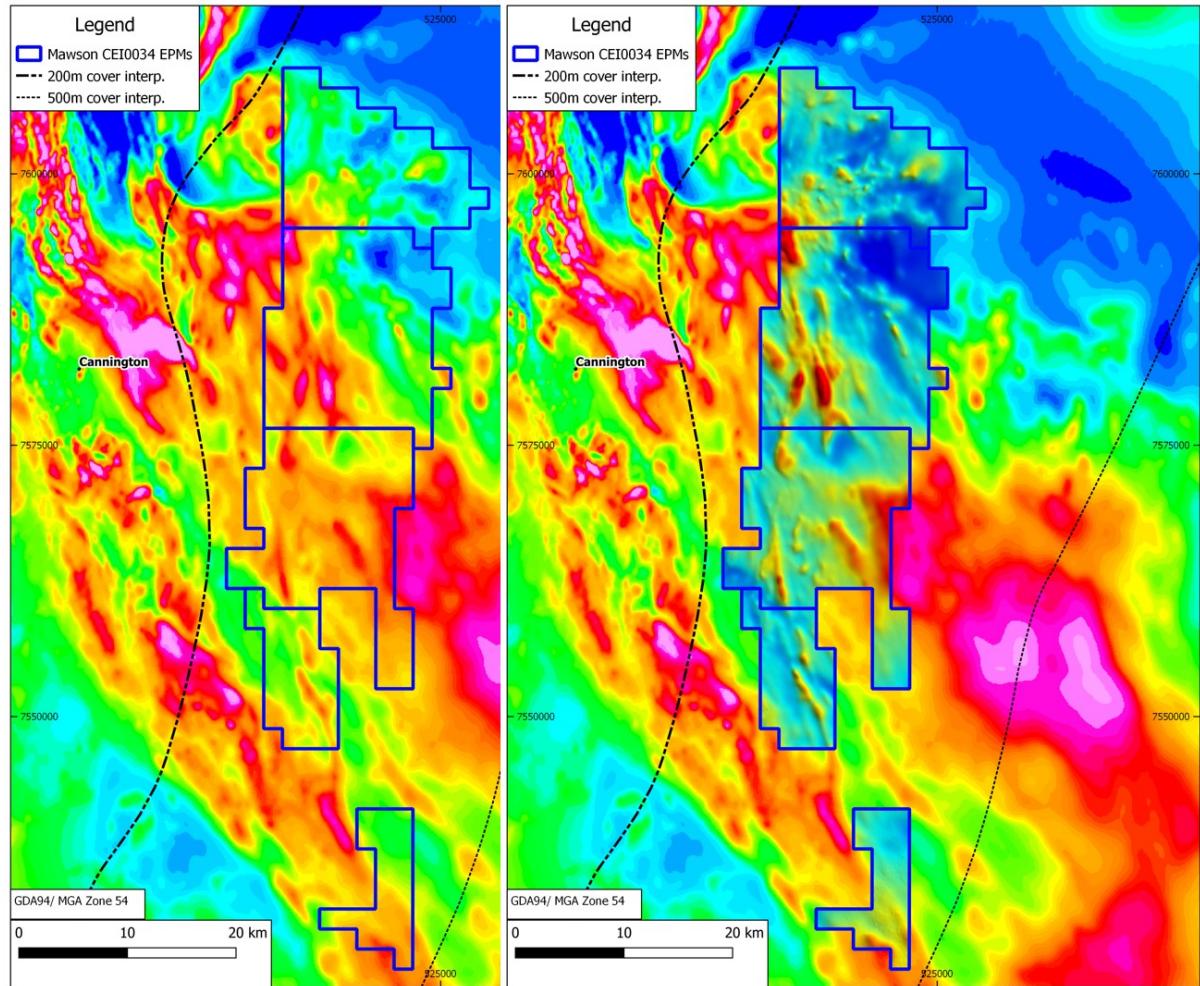


Figure 6. RTP pseudocolor magnetics.

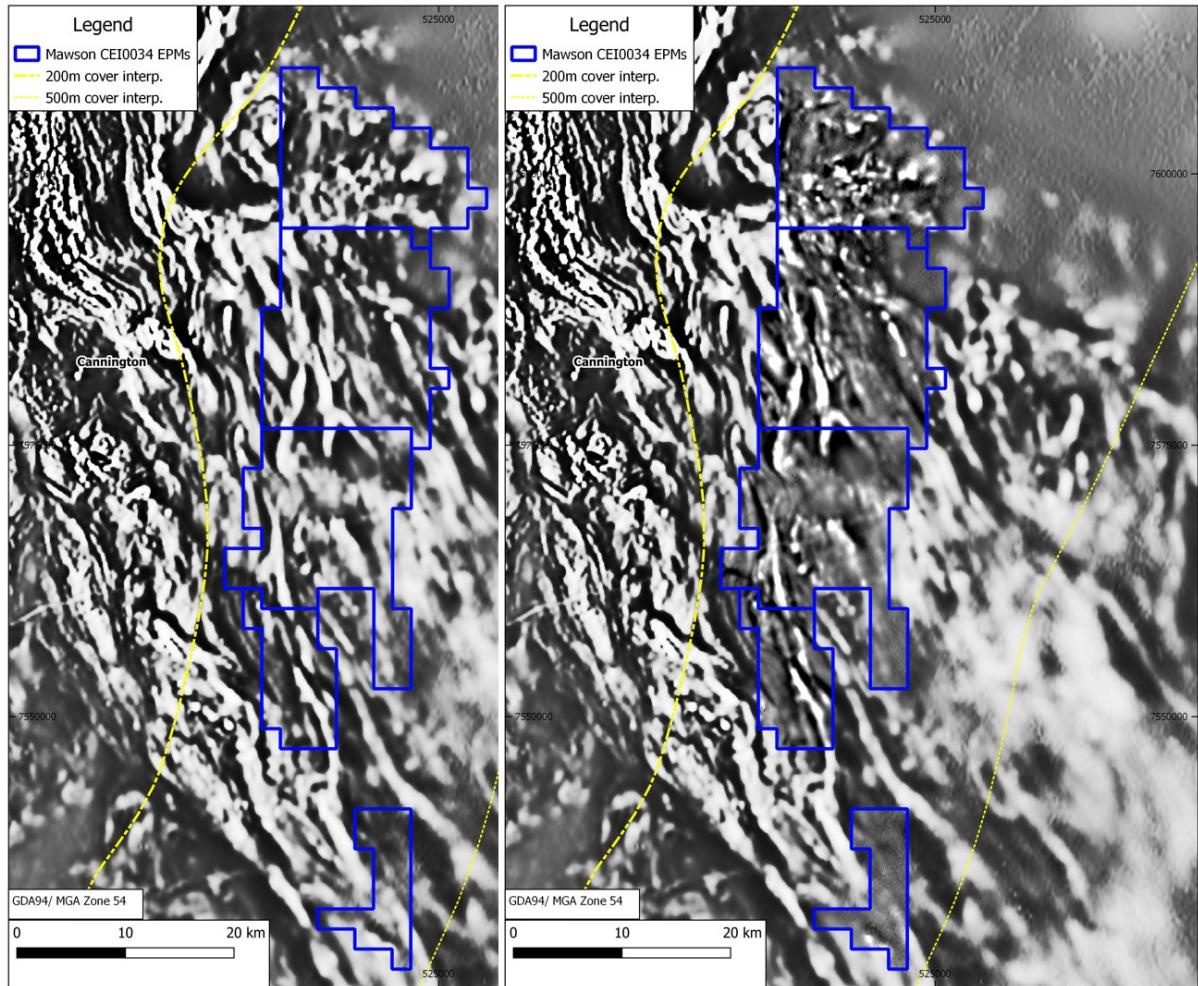


Figure 7. RTP 1VD greyscale magnetics.

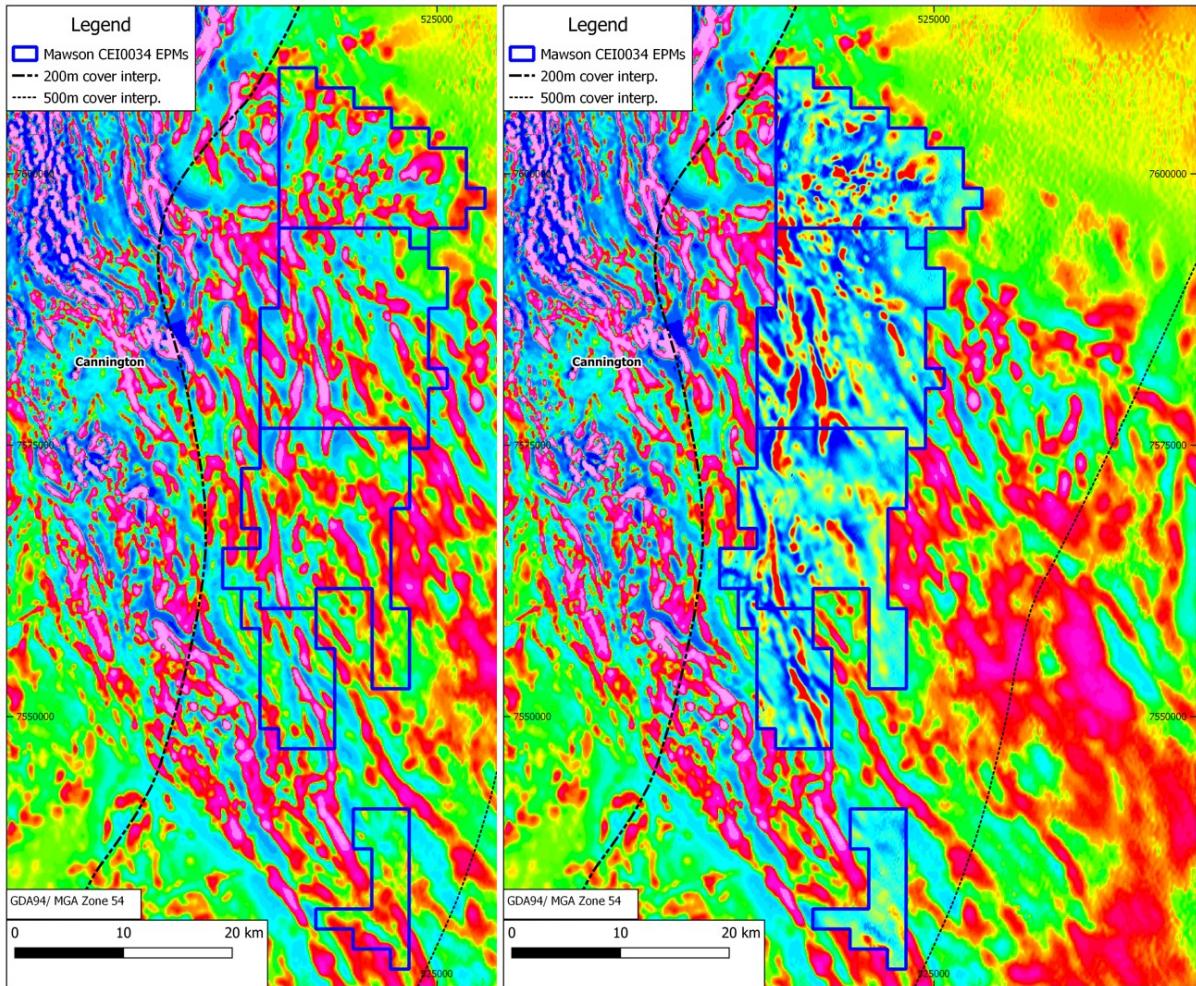


Figure 8. RTP 1VD pseudocolor magnetics.

### Ground gravity

Preliminary processing of the new ground gravity data was undertaken by Robert Smith of Greenfields Geophysics. This included generation of geoTiff images of Bouguer anomaly and first vertical derivative of Bouger anomaly (Figures 9 and 10 respectively).

Initial attempts to grid this new gravity data are challenged by (i) the irregular shape of the CEI tenements and (ii) the relatively wide 1 km spacing of the gravity stations. A current compromise is application of an upward continuation (UC200) which smooths the data prior to generating a first vertical derivative. The net result, as shown in Figure 10, has removed many of the regional long wavelength features which tend to obscure features of interest.

While interpretations may be an artefact of the gridding process, the new gravity data suggest greater density heterogeneity. This is within and on the margins of the broad high-gravity domain that occupies the central and northern parts of the CEI tenements. This domain may be related to basalts in the Toole Creek volcanics interpreted east of the Cloncurry fault zone (Figure 2). Alternatively the gravity high may reflect exhumation of denser rocks of higher metamorphic grade.

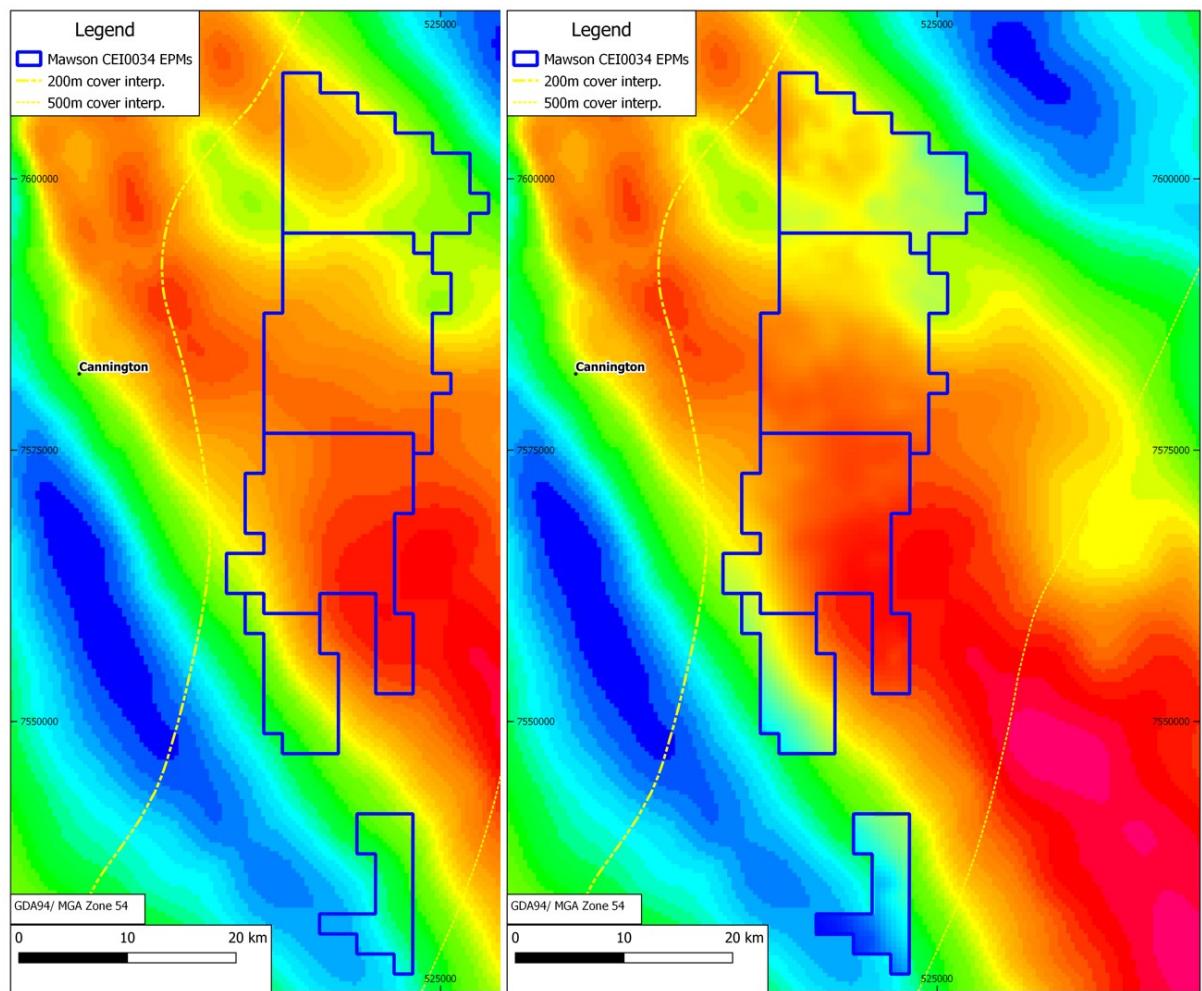


Figure 9. Ground gravity Bouguer anomaly. LHS = existing 4km grid-spaced data. RHS within CEI tenements = 1km grid-spaced data Bouguer anomaly with upward continuation (UC200).

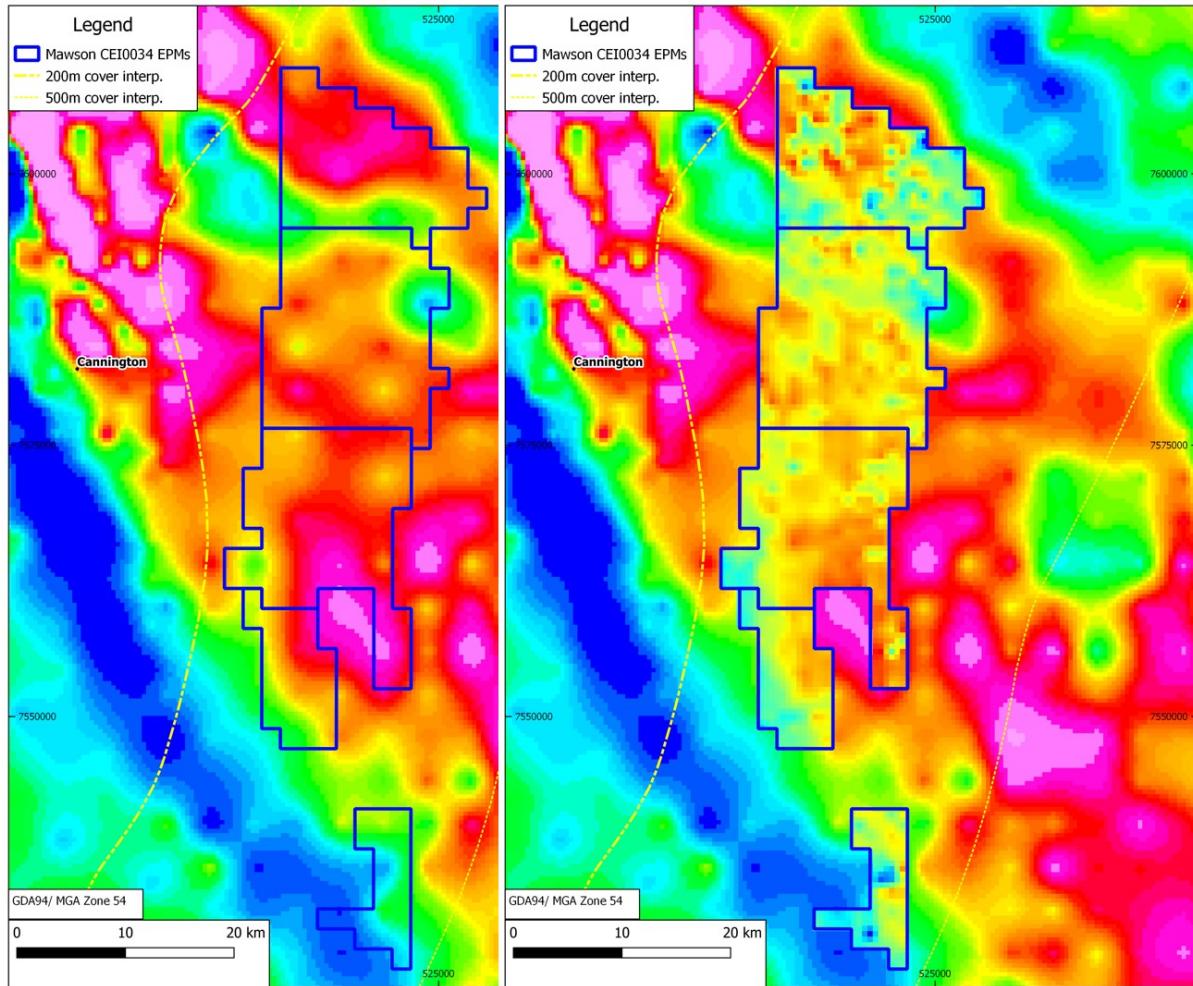


Figure 10. Ground gravity 1VD of Bouguer anomaly. LHS = existing 4km grid-spaced data. RHS within CEI tenements = 1km grid-spaced data Bouguer anomaly with upward continuation (UC200) then 1VD.

## 10. Overall Comments

The ground gravity and aeromagnetic surveys were completed without incident and provide valuable additional data to Mawson's Isa SE project. These new data represent the first step in progressing this early-stage conceptual project towards a next phase of interpretation and subsequent targeting.

Additional geophysical processing and lithostructural interpretation of the combined potential field datasets is planned for later in 2019. This work will refine existing interpretations of basement lithology and architecture. It may also highlight areas that require infill gravity or magnetic surveying.

The lithostructural interpretation will enable a first-principles structural-stratigraphic approach to targeting. This will include recognition of favourable host sequences and their relationship to major and second order structures. This approach will complement the identification of non-stratigraphic magnetic-gravity highs.

## **11. References**

- Austin, J.R., Gazley, M.F., Walshe, J.L. and Patterson B.O. 2016. Uncover Cloncurry – Summary Geophysical Expressions of the Cloncurry Mineral System. CSIRO report EP166451, Australia, pp. 21.
- Hinman, M. 2018. Solid geology interpretation of the southern Eastern Fold Belt, Mt Isa, Northwest Queensland. University of Queensland WH Bryan Mining and Geology Research Centre.
- Spampinato, G.P.T., Betts, P.G., Ailleres, L. and Armit, R.J., 2015. Structural architecture of the southern Mount Isa terrane in Queensland inferred from magnetic and gravity data. Precambrian Research, 269, pp.261-280.
- Witherly, K. and Mackee, G., 2015. Geophysical Responses over the Cannington Ag-Zn-Pb Deposit, Queensland. ASEG Extended Abstract, 2015, 1-5.

## **12. Appendices**

Appendix 1 - Aeromagnetics operations report (Thomson Aviation)

Appendix 2 - Ground gravity operations report (Haines Geophysical Surveys)

Appendix 3 - Digital data cover sheet

# Mawson Canada Pty Ltd

## Airborne Geophysical Survey Operations Report

Isa SE

**THOMSON AVIATION**  
Airborne Geophysical Survey



Thomson Aviation Job  
F18063





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# PART 1 - SPECIFICATIONS FOR AIRBORNE GEOPHYSICAL SURVEY

## 1.1 SURVEY DETAILS

Start Date	13/04/2019
End Date	22/04/2019
Time Base - Magnetics	20 Hz
Time Base - Radiometrics	2 Hz
Base Mag Locations	Cloncurry
Ground Cals Locations	Cloncurry
Test Line Locations	Cloncurry
Block 1	North Block
Block 2	South Block
Total Processed Line Kilometers	7812.4



## 1.2 LOCATION MAP

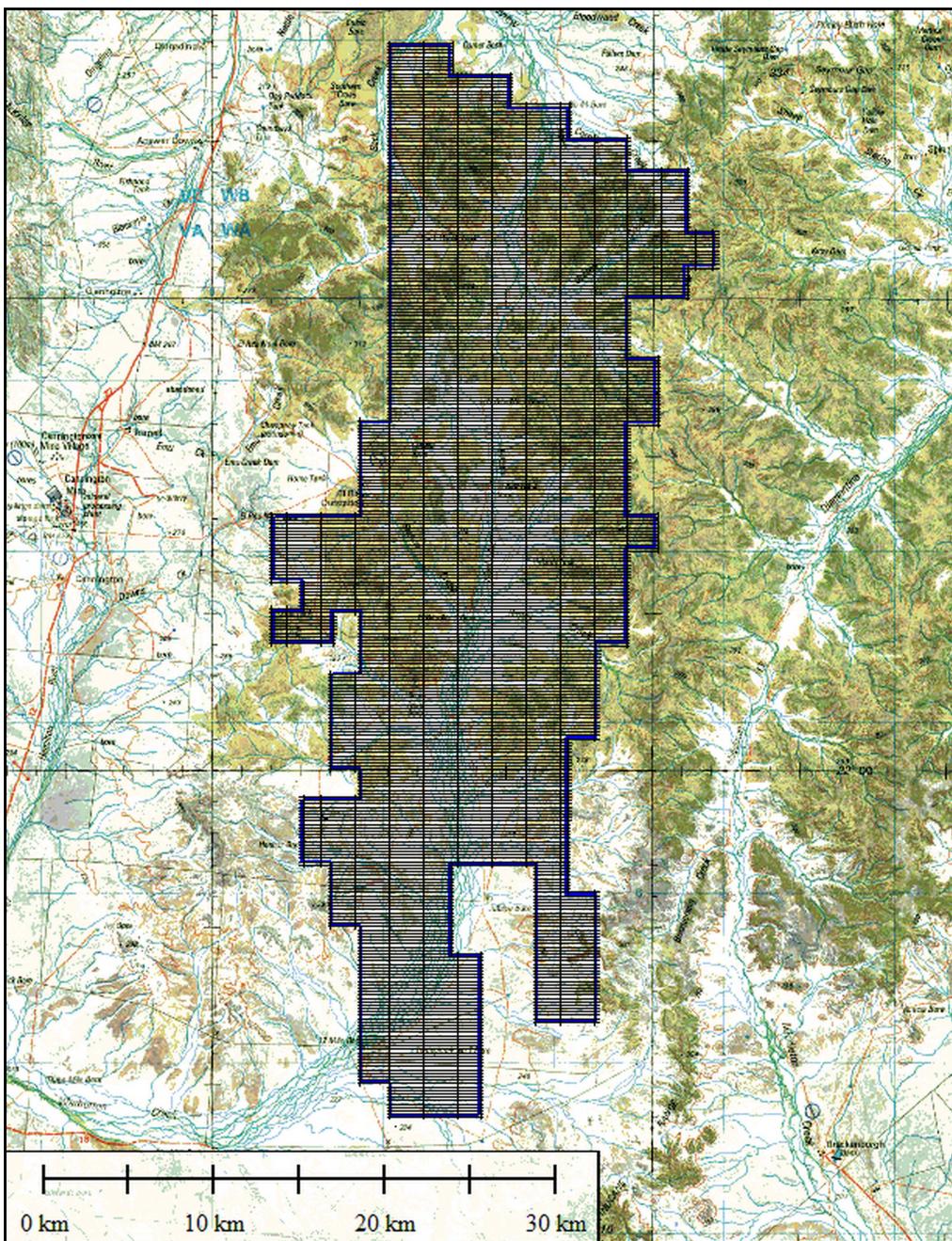


Figure 1 Isa SE



## 1.3 SURVEY SPECIFICATIONS

North Block	
Traverse line direction	90
Traverse line spacing	200 m
Tie line direction	180
Tie line spacing	2000 m
Block Traverse Kilometers	4,683
Block Tie Kilometers	559
Block Total Kilometers	5,242
Mean terrain clearance (m)	40

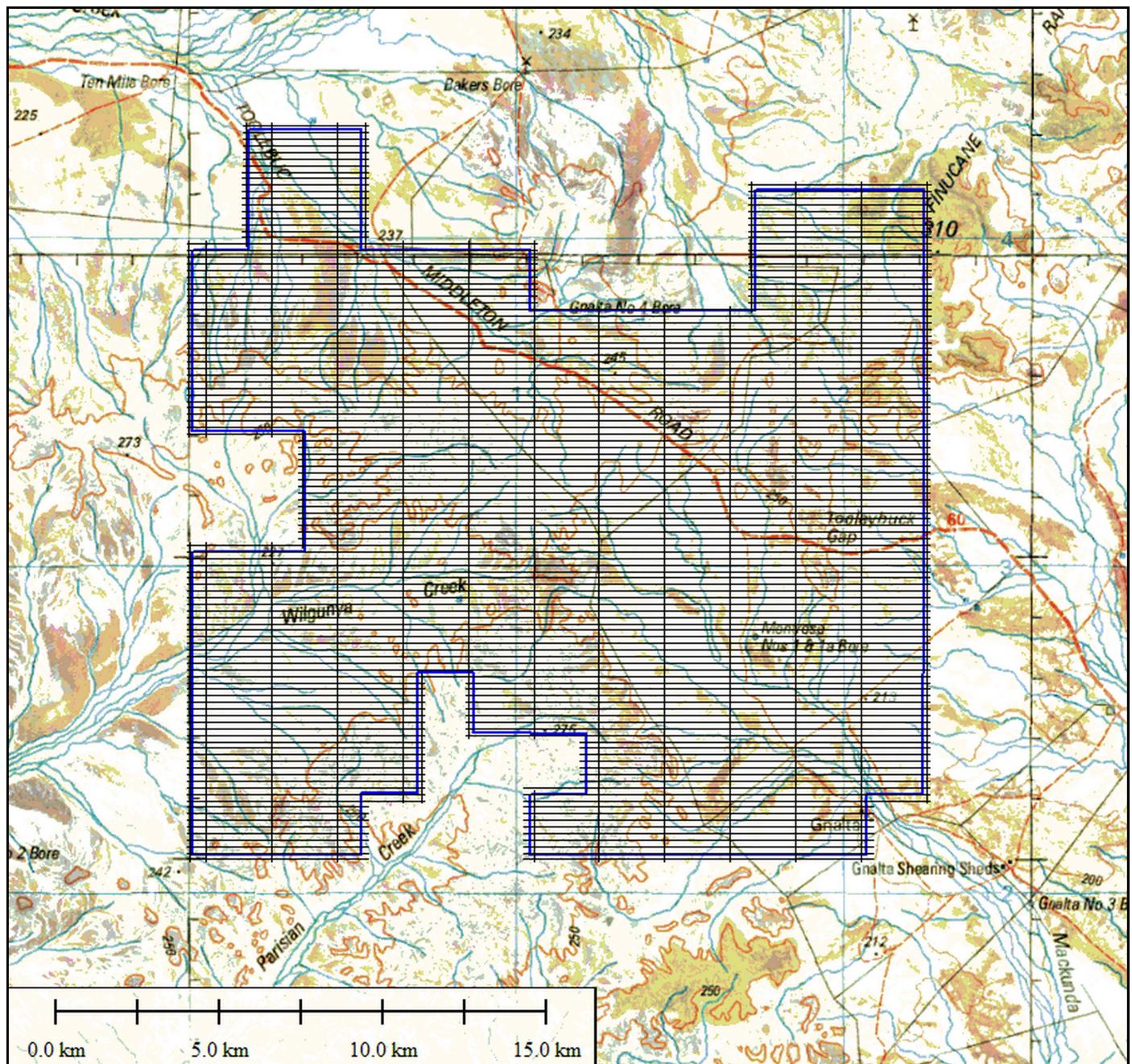


**Figure 2** North Block



## **SURVEY SPECIFICATIONS (Cont)**

South Block	
Traverse line direction	90
Traverse line spacing	200 m
Tie line direction	180
Tie line spacing	2000 m
Block Traverse Kilometers	2,207
Block Tie Kilometers	271
Block Total Kilometers	2,478
Mean terrain clearance (m)	40



**Figure 3** South Block



## **1.4 CALIBRATION RANGE**

The radiometric systems for each aircraft were calibrated using the Geoscience Australia calibration range in Carnamah WA to determine the ground concentration coefficients for the radiometric systems.

Cosmic stacks were flown over water to determine the aircraft and cosmic coefficients.

Height attenuation coefficients were determined from IAEA recommended attenuation coefficients.

## **1.5 IN FIELD CALIBRATION**

### **a) Spectrometer**

The gamma ray spectrometer response was verified by exposing the system to thorium test samples for a time sufficient to accumulate 10,000 counts.

Frequency      Before the first flight and after the last flight of each day when survey operations were conducted.

All background corrected counts fell within +/- 3% of the mean over the survey period.

Results of thorium test sample measurements can be found in Appendix B and Appendix C.

### **b) Test Line**

Test lines are flown at the specified survey height to verify magnetometer, spectrometer and barometric altimeter baselines.

Length            10km

Direction        Bi-Directional

Frequency        Before the first flight and after the last flight of each day when survey operations were conducted.

The test line thorium counts fell within +/- 7% of the mean over the survey period.

Results of test line thorium counts can be found in Appendix B and Appendix C

### **c) Compensation Flight**

Compensation flights for all aircraft were carried out to determine how aircraft manoeuvring effects affected the magnetic data. These aircraft induced effects are then removed from the collected magnetic data during data processing.

Frequency        Before the commencement of the survey project and after each scheduled maintenance operation.



## **1.6 IN FIELD VERIFICATION AND PROCESSING**

Thomson Aviation conducts stringent real time data validity checks.

The following products were generated on site utilising ChrisDBF and Geosoft database programs as well as Thomson Aviation proprietary software:

- Flight path plots, to demonstrate quality of navigation
- Magnetic stacked profiles, to demonstrate character of magnetic data
- Statistical summary of line data
- Magnetometer base station plots
- Progressive image presentation of magnetic and topographic data
- Daily plots of aircraft parking locations to verify GPS position

## **1.7 NAVIGATION AND POSITIONING**

Navigation was provided using a mobile Novatel OEMV-1 VBS receiver. This equipment provides flight guidance to the pilot as well as flight path information which was recorded for subsequent processing.

Differential GPS data was obtained in real time using static GPS data obtained from the Omnistar wide area GPS service.

Position relative to the survey line was displayed to the pilot by an accurate and effective system proprietary to Thomson Aviation.

Under normal circumstances differential GPS is expected to yield positional accuracies in the order of 5 meters RMS or better.



## PART 2 - AIRCRAFT

The aircraft used for survey operations combine good manoeuvrability with a magnetically clean base to provide maximum magnetic sensor performance.

### 2.1 VH-SUX

Aircraft Information	
Engine	Piston
Fuel	AVGAS
Fuel Burn	65 litres per hour
Typical Survey Speed	130 knots
Stall Speed	60 knots

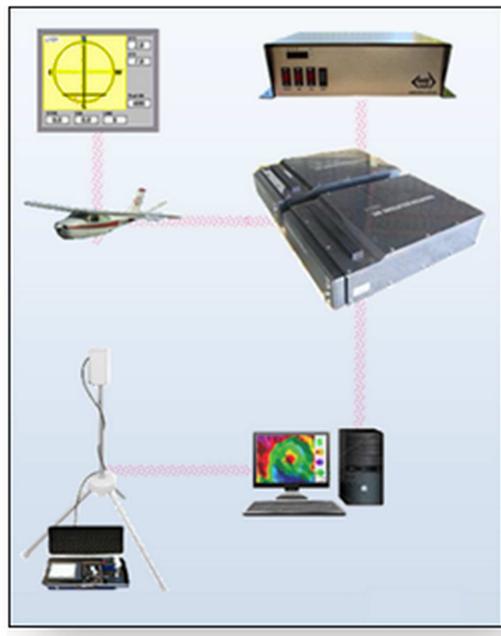


**Figure 4** Example Aircraft: Cessna C210





## PART 3 - SURVEY INSTRUMENTATION



**Figure 5** System Outline

### 3.1 MAGNETOMETER

The Geometrics G822A Magnetometer is a highly sensitive unit incorporating an optically pumped sensor. The constant harmonic frequency from the sensor is proportional to the surrounding scalar magnetic field. This frequency is resolved by the Counter / Processor which provides the magnetic field to a nominal accuracy of 0.01nT with a data capture rate of 20 times per second both in analog and digital formats.

The sensor and pre-amp are mounted in a stinger assembly which may be attached to the front or rear of the survey aircraft.



**Figure 6** G822A Magnetometer and Typical Stinger Mounts



## 3.2 RADAR ALTIMETER

Type: King KR 495B Radar Altimeter



**Figure 7** Radar Altimeter

This unit is a high resolution, short pulse ratio altitude system designed for automatic continuous operation over wide variations of terrain and weather conditions, target reflectivity, and aircraft altitude. It provides an accurate terrain clearance indication ranging from 0 to 650m (0 to 2,000ft).

## 3.3 BAROMETRIC ALTIMETER

Type: Setra 276 Pressure Transducer



**Figure 8** Pressure transducer

This type of pressure transducer operates over a range of 600 to 1100 mB and its resolution is limited only by system noise. The sensor is referenced to the height given by the GPS.

## 3.4 DATA ACQUISITION SYSTEM

Type: GeOZ-DAS Digital Data Acquisition System



**Figure 9** Zdas System

The GeOZ system manages the data acquisition and saves the data to removable Flash Cards.

It provides guidance and real time error diagnostics for the pilot.

Acquired data is transferred to a field computer on completion of the flight for both verification and archiving prior to being shipped to the processing centre.



## 3.5 NAVIGATION EQUIPMENT

Type: Novatel OEMV-1VBS GPS Receiver

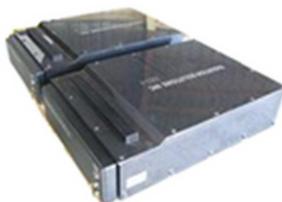


**Figure 10** GPS Receiver

This equipment is a 12 channel parallel tracking receiver capable of providing sub-meter resolution at 5Hz and is integrated with the GeOZ-DAS acquisition unit.

## 3.6 GAMMA RAY SPECTROMETER SYSTEM

Type: Radiations Solutions Inc. RS 400 Spectrometer



**Figure 11** RS 400 Systems

These units deliver high-resolution spectral information from 0.33 MeV to 3.0 MeV including the five primary regions of interest; Total Count, Potassium, Uranium, Thorium and Cosmic.

The Gamma Ray Spectrometer is interfaced to a NaI (TI) crystal detector pack with a total volume of 33 liters (2048 cubic inches). These detector packs embody the latest techniques whereby the elimination of dead time in the counting process yields up to 30% more counts over other commercial systems.

Superior calibration facilities included the visual real time monitoring of full spectrum data and in flight monitoring of gain drift relative to the selected isotope window maintain long-term data quality.

Enhancement of the spectrometer data is achieved by noise reduction techniques (NASVD or MNF), followed by dead time correction, energy calibration, cosmic/aircraft background correction and atmospheric radon removal all applied to the 256 channel data. Spectral stripping, height correction and conversion to radio-element concentrations are then applied prior to gridding and micro-levelling.

The gamma ray spectrometer response was verified by exposing the system to thorium test samples for a time sufficient to accumulate 10,000 counts.



### 3.7 BASE STATION MAGNETOMETER

Two units are used in tandem for diurnal monitoring. These units run continuously during the survey periods and record the data in digital format.

Base station magnetometer instruments record data to a sensitivity of 0.1nT every 6 seconds.

During data acquisition, if the non-linear diurnal variation was greater than 10 nT in 10 minutes, or the deviation from a straight line chord of length 10 minutes exceeded 10 nT, the line was reflown.



**Figure 12** Setting up base station magnetometer

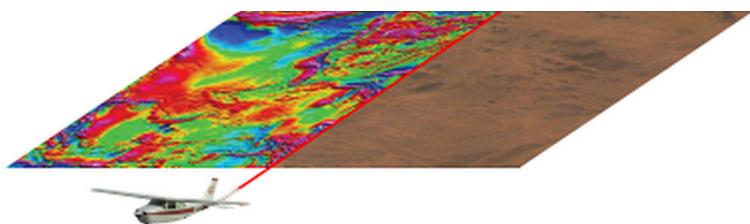


**Figure 13** Magnetometer and Data Console



## PART 4 - CONTACT INFORMATION

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## **PART 5 - APPENDICES**

### **APPENDIX A**

### **DAILY REPORTS**





Daily Log								
Date	Fit Num	Block(s)	Operator(s)	Aircraft	SBY	MINT	SUS	Comments
13/04/2019		North Block		VH-SUX				Aircraft ferried from Griffith to Wagga Wagga.
13/04/2019		North Block		VH-SUX				Aircraft ferried from Wagga to Charleville.
13/04/2019		South Block		VH-SUX				Aircraft ferried from Charleville to Cloncurry
14/04/2019		North Block		VH-SUX				Recces flight completed over survey areas to identify additional hazards not considered during additional risk assessment. Recce identified not additional hazards and confirmed proposed survey altitude of 40m AGL.
14/04/2019	1	South Block	R Butterfield	VH-SUX				Comptoboxes completed in preparation for the start of survey flying.
15/04/2019	2	South Block	R Butterfield	VH-SUX				L20001.0 - T20019.0 and T29001.0 - T29003.0 flown and all data accepted.
15/04/2019	3	South Block	R Butterfield	VH-SUX				L20020.0 - 20057.0 flown and all data accepted.
16/04/2019	4	South Block	R Butterfield	VH-SUX				L20058.0 - L20085.0 and T29004.0 - T29006.0 flown and all data accepted.
16/04/2019	5	North Block	R Butterfield	VH-SUX				L20086.0 - L20122.0, T29007.0 - T29017.0 and L10001.0 - L10011.0 flown and all data accepted
17/04/2019	6	North Block	R Butterfield	VH-SUX				L10012.0 - L10058.0 and T19001.0 - T19006.0 flown and all data accepted
17/04/2019	7	North Block	R Butterfield	VH-SUX				L10057.0 - L10113.0 and T19007.0 - T19008.0 flown and all data accepted.
18/04/2019		North Block		VH-SUX				Aircraft taken to Mt Isa for oil and filter change as part of the scheduled maintenance program post new engine installation
18/04/2019		North Block				0.5		Aircraft in scheduled maintenance.
18/04/2019		North Block		VH-SUX				Aircraft returned to Cloncurry
18/04/2019	8	North Block	R Butterfield	VH-SUX				L101140.0 - L101390 and L10179.0 - L10193.0 flown and all data accepted.
19/04/2019	9	North Block	R Butterfield	VH-SUX				L10149.0 - L10177.0 and T19016.0 - T19022.0 flown and all data accepted.
19/04/2019	10	North Block	R Butterfield	VH-SUX				L10140.1 - L10212.0 and T19015.0, T19017.0, T19020.0 flown and all data accepted. First flight attempt was aborted due to a software problem with the RSI packs, this was resolved and the flight continued without issue.
20/04/2019	11	North Block	R Butterfield	VH-SUX				L10213.0 - L10245.0 and T19010.0 - T19014.0 flown and all data accepted.



Daily Log						
Date	Fit Num	Block(s)	Operator(s)	Aircraft	SBY	SUS
20/04/2019	12	North Block	R Butterfield	VH-SUX		L10246.0 - L10248.0 flown and data accepted. The flight was aborted after a powers supply failure to 1 of the crystal packs.
22/04/2019	13	North Block	R Butterfield	VH-SUX		L10249.0 - L10316.0 flown and all data accepted.

**APPENDIX B**

**CALIBRATION AND TEST LINE VARIATION TABLES**



Ground Cals - VH-SUX - Cloncurry																				
Date	Position			Hand Sample			Background			Normalized			Th Cal Results							
	Fit	East	North	GPS Ht	TC	Pot	Ura	Tho	TC	Pot	Ura	Tho	% F WHM	+/- 3%	5 max					
15/04/2019	2	448640.65	7714458.52	190.6	8781.6	591.1	229.3	437.0	469.5	126.5	156.5	4147.1	121.6	280.5	218.87	4.46	0.0	0.0		
15/04/2019	3	448640.91	7714457.36	189.2	8575.2	575.7	212.6	412.7	4567.9	443.6	119.0	147.6	4007.3	132.1	93.6	265.1	213.31	5.05	-2.8	1.2
16/04/2019	4	448640.98	7714457.76	188.6	8829.9	596.4	231.3	435.3	4707.0	473.7	130.4	156.7	4122.9	122.7	100.9	278.6	218.58	4.50	1.4	0.8
16/04/2019	5	448641.48	7714457.25	189.6	8586.2	585.5	209.9	411.5	4522.0	444.8	117.8	143.9	4064.2	140.7	92.1	267.6	213.19	5.13	-2.0	1.5
17/04/2019	6	448641.69	7714457.53	188.8	8771.4	595.8	223.1	436.7	4590.5	463.6	124.1	153.5	4180.9	132.2	99.0	283.2	218.39	4.54	3.0	1.4
17/04/2019	7	448640.86	7714457.39	189.0	8614.9	579.1	209.7	408.8	4587.2	442.2	119.7	146.5	4027.7	136.9	90.0	262.3	212.76	5.22	-3.9	1.1
18/04/2019	8	448641.54	7714457.48	189.5	8707.8	598.5	219.9	431.2	4580.3	462.3	120.7	150.9	4127.5	136.2	99.2	280.3	212.76	5.18	2.3	1.4
18/04/2019	8	448641.42	7714457.02	189.8	8547.3	580.0	207.3	407.9	4485.1	438.0	114.4	142.3	4062.2	142.0	92.9	265.6	212.76	5.18	-2.7	1.7
19/04/2019	9	448641.51	7714457.33	189.3	8667.7	587.9	221.3	430.2	4556.8	464.9	122.7	151.2	4110.9	123.0	98.6	279.0	217.49	4.46	2.0	1.5
19/04/2019	10	448640.81	7714457.45	188.8	8796.1	592.6	224.7	437.0	4656.4	473.2	128.5	156.0	4139.7	119.4	96.2	281.0	217.67	4.52	2.4	1.1
20/04/2019	11	448641.47	7714458.12	189.5	8765.9	590.3	224.0	428.4	4670.5	471.1	128.4	156.6	4095.4	119.2	95.6	271.8	217.67	4.55	-0.8	0.9
22/04/2019	13	448641.08	7714457.78	188.7	9044.5	609.1	244.4	432.0	4938.6	485.9	143.5	154.1	4105.9	123.2	100.9	277.9	217.72	4.53	1.3	0.9
22/04/2019	13	448640.81	7714457.01	189.7	8906.7	603.4	235.0	435.1	4770.1	478.0	133.8	157.1	4136.6	125.4	101.2	278.0	217.72	4.53	1.2	1.5



Test Lines - VH-SUX - Cloncurry												
	801				802							
Date	Fit	TC	Pot	Ura	Tho	TH Chg	Fit	TC	Pot	Ura	Tho	TH Chg
15/04/2019	2	2089.0	209.8	54.1	67.6	0.0	3	2020.1	197.7	51.1	63.8	-2.9
16/04/2019	4	2137.2	214.2	57.7	69.4	3.7	5	2048.3	197.4	52.4	64.6	-2.6
17/04/2019	6	2082.9	210.3	55.4	68.4	2.5	7	2034.4	195.9	51.7	64.1	-3.3
18/04/2019							8	2063.0	200.7	52.6	64.7	-2.1
19/04/2019	9	2120.8	214.5	56.4	68.2	2.8	10	2066.9	210.7	52.8	67.7	1.8
20/04/2019	11	2143.7	217.3	56.4	70.1	4.8						
22/04/2019	13	2338.6	224.5	71.0	69.1	3.0	13	2200.2	213.2	66.4	69.7	3.6

## **APPENDIX C**

## **CALIBRATION AND TEST LINE VARIATION CHARTS**

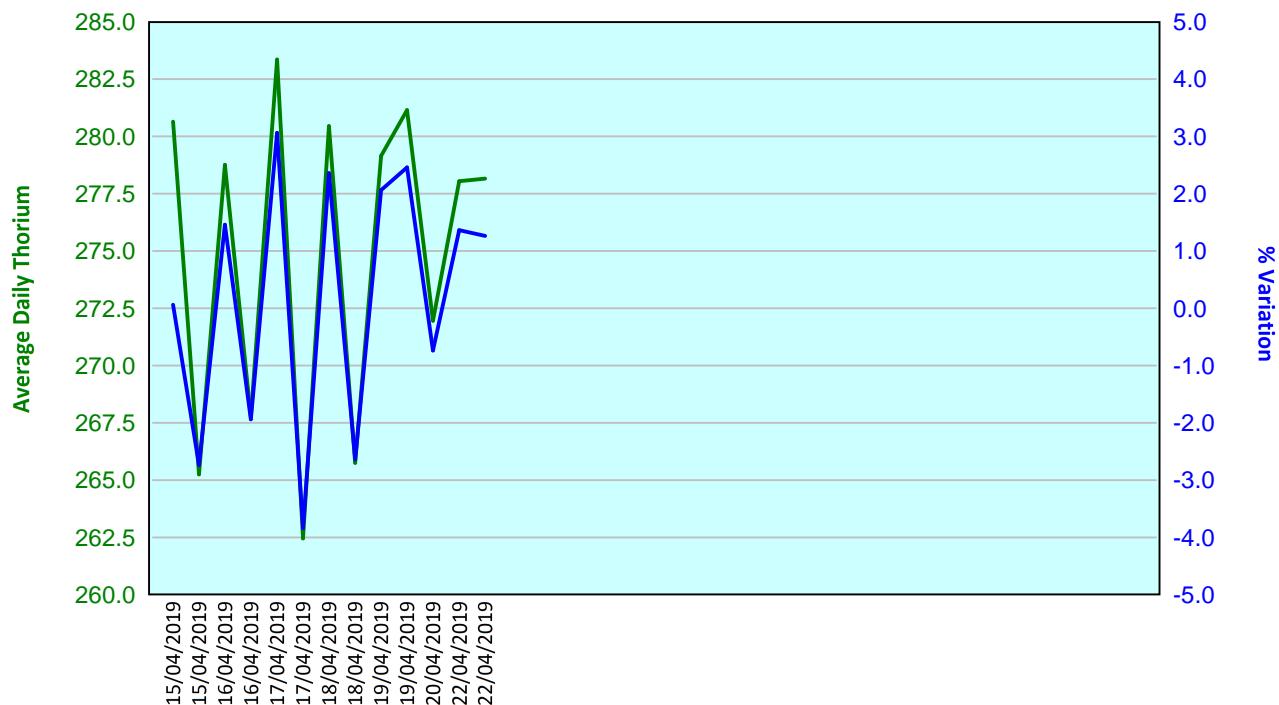




### Sample Variations

Aircraft: VH-SUX Base: Cloncurry

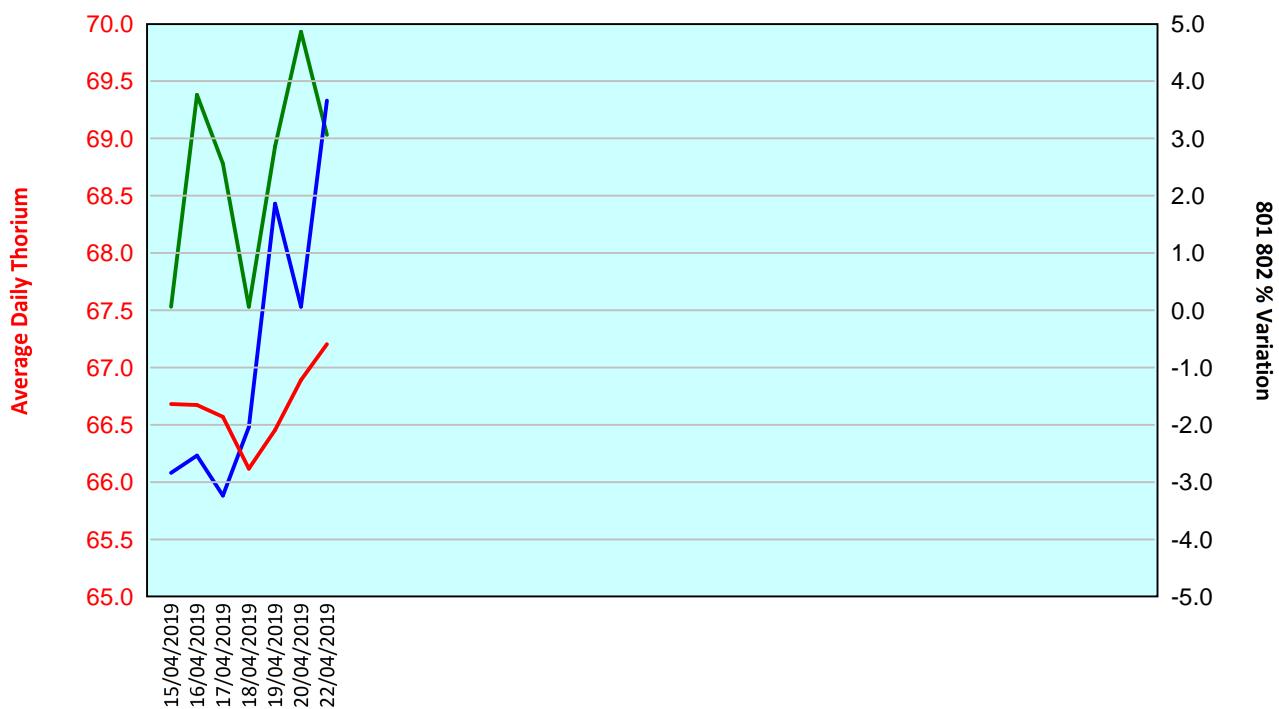
Norm Tho  
% Var



Aircraft: VH-SUX Base: Cloncurry

Test Line Variations

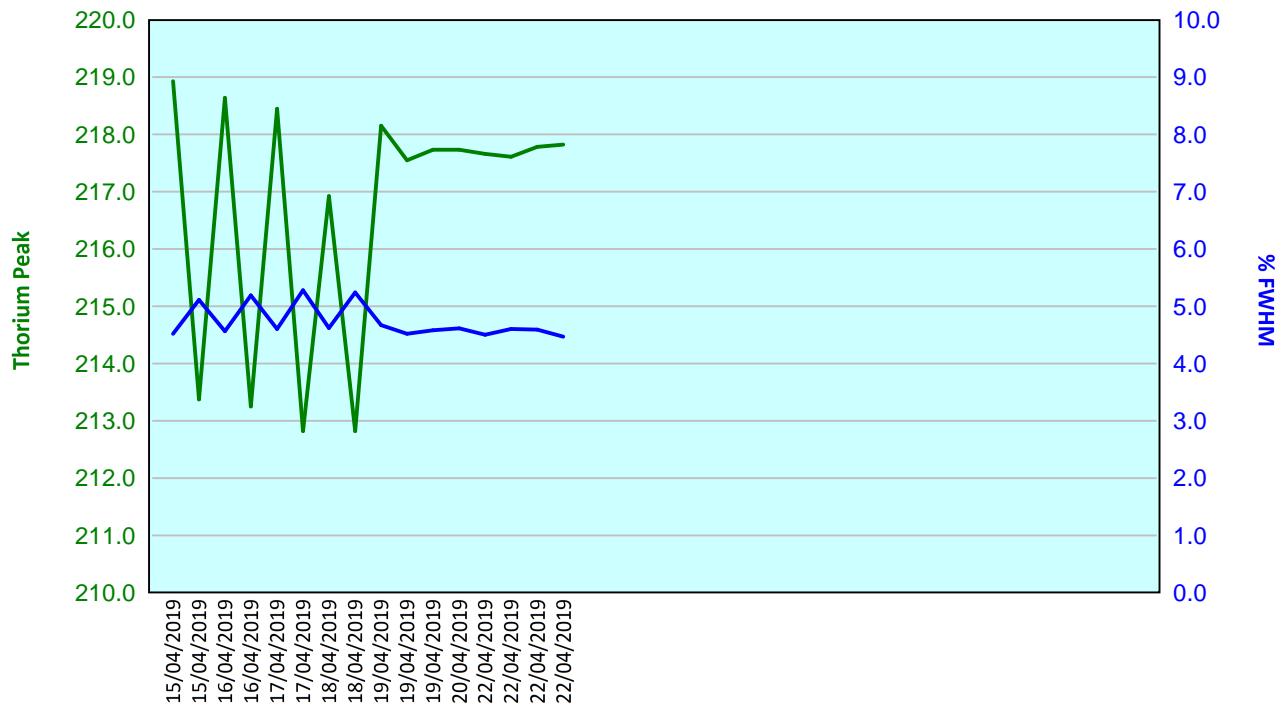
TH Chg 801 — 802 —  
Norm Tho —



### Thorium Calibration Results

Aircraft: VH-SUX

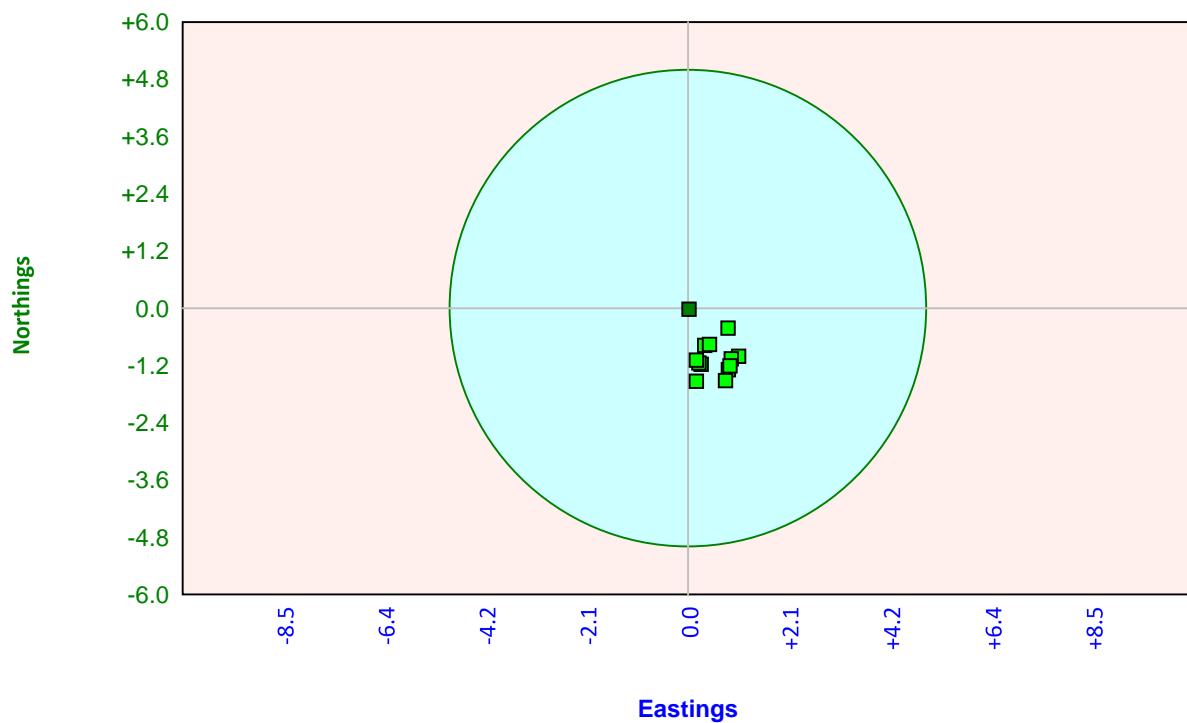
ThPeak —  
% FWHM —



### Hand Sample Calibration Positions

Aircraft: VH-SUX Base: Cloncurry

Normal	[Green Square]
Error (>5)	[Red Square]



## **APPENDIX D**

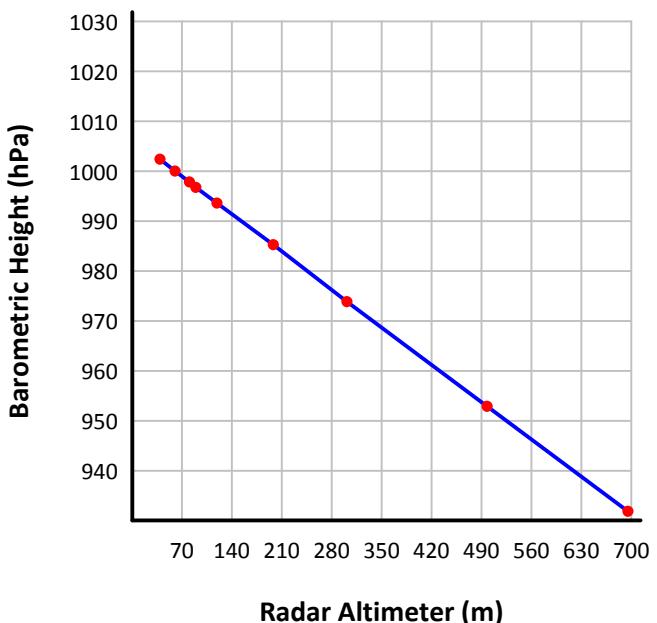
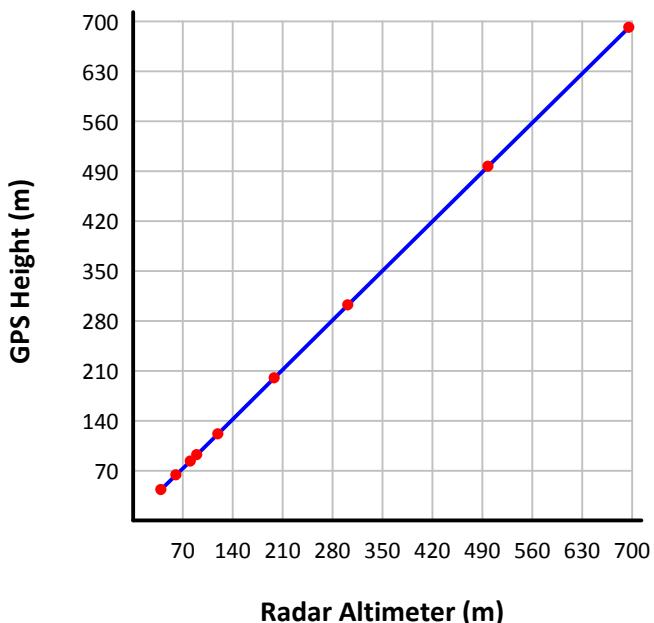
### **RADAR ALTIMETER AND BAROMETRIC ALTIMETER CHECKS**





# VH-SUX

Radar Altimeter (m)	Barometric Height (hPa)	GPS Height (m)
39.25	1002.41	43.51
60.44	999.99	63.82
80.71	997.83	83.44
89.53	996.74	92.44
119.14	993.63	121.58
198.27	985.23	199.82
301.44	973.86	302.32
498.06	952.86	496.68
695.87	931.83	691.58



Calibration flights for VH-SUX were performed within the last 12 months





## **APPENDIX E**

## **BOUNDARY COORDINATES**





**North Block, Datum: GDA 94, Zone: 54**

Eastings	Northings	Eastings	Northings
510469.58	7609764.16	515583.44	7547038.60
513919.44	7609761.57	510428.86	7547042.90
513917.85	7607916.87	510430.04	7548887.71
517367.31	7607913.54	508711.64	7548888.77
517365.32	7606068.84	508716.53	7558112.77
520814.38	7606064.77	506997.10	7558113.64
520811.98	7604220.06	506998.64	7561803.22
524260.69	7604215.26	505278.81	7561803.90
524257.90	7602370.54	505280.09	7565493.40
527706.21	7602364.98	508720.53	7565491.86
527699.83	7598675.54	508721.56	7567336.60
529423.60	7598672.48	507001.14	7567337.47
529420.21	7596827.76	507003.65	7572871.68
527696.64	7596830.82	508724.65	7572870.83
527693.45	7594986.09	508726.70	7576560.29
524246.71	7594991.66	507005.31	7576561.14
524241.22	7591302.21	507004.48	7574716.41
525964.19	7591299.51	505283.28	7574717.08
525958.30	7587610.06	503562.12	7574717.56
524235.74	7587612.74	503562.55	7576562.28
524227.49	7582078.52	505283.91	7576561.80
525949.44	7582075.83	505284.55	7578406.52
525946.48	7580231.08	503562.98	7578407.01
524224.73	7580233.78	503563.40	7580251.74
524216.37	7574699.52	503563.82	7582096.48
522495.26	7574702.06	505285.80	7582095.00
522487.50	7569167.76	507007.77	7582095.34
520766.89	7569170.12	508729.74	7582094.49
520754.95	7559946.26	508732.75	7587628.68
522474.44	7559943.86	510455.31	7587627.65
522469.22	7556254.28	510469.58	7609764.16
522464.00	7552564.68		
519026.47	7552569.22		
519035.28	7559948.39		
519037.47	7561793.17		
513877.97	7561798.61		
513873.20	7556264.25		
515592.43	7556262.62		



**South Block, Datum: GDA 94, Zone: 54**

Eastings	Northings	Eastings	Northings
500119.87	7530442.93	510412.87	7523060.12
501836.19	7530442.84	512128.38	7523058.88
503552.50	7530442.56	512129.80	7524903.73
503552.90	7532287.40	510414.09	7524904.97
503553.31	7534132.23	508698.39	7524906.03
501836.57	7534132.52	508699.40	7526750.88
500119.84	7534132.61	506983.50	7526751.74
500119.84	7535977.45	506982.69	7524906.89
500119.82	7537822.28	506981.87	7523062.04
500119.81	7539667.11	505266.37	7523062.71
501837.16	7539667.01	505265.76	7521217.86
501837.36	7541511.83	503550.50	7521218.31
501837.56	7543356.65	501835.23	7521218.57
503555.32	7543356.35	500119.96	7521218.64
505273.10	7543355.87	500119.94	7523063.51
505272.48	7541511.05	500119.93	7524908.37
505271.87	7539666.24	500119.90	7526753.23
506989.24	7539665.56	500119.88	7528598.08
508706.60	7539664.70		
510423.97	7539663.64		
510422.72	7537818.82		
512139.88	7537817.58		
513857.04	7537816.15		
515574.20	7537814.53		
517291.36	7537812.72		
517295.50	7541502.36		
522448.17	7541495.81		
522426.71	7526737.12		
522424.07	7524892.26		
522421.43	7523047.41		
520705.90	7523049.80		
520703.46	7521204.94		
518988.15	7521207.14		
517272.85	7521209.15		
515557.56	7521210.96		
513842.25	7521212.59		
512126.95	7521214.02		
510411.65	7521215.27		



## **APPENDIX F**

## **LINE SPECIFICATIONS**





## Line Specifications Header Descriptions

Line	Line number
Type	Traverse or tie line
Easting	Line start easting co-ordinate
Northing	Line start northing co-ordinate
Easting	Line end easting co-ordinate
Northing	Line end northing co-ordinate
Direc	Line orientation (Degrees)
Length	Individual line length (km)
Tv Cumul	Traverse lines total cumulative distance (km)
Ti Cumul	Tie lines total cumulative distance (km)













### North Block (Cont)

Line	Type	Easting	Northing	Easting	Northing	Direc	Length	Tv	Cumul	Ti	Cumul
190100	Tie	517453.61	7608143.80	517453.61	7606184.90	180.0	2.0	4682.8	223.9		
190110	Tie	516327.32	7608153.44	516327.32	7552385.94	180.0	55.8	4682.8	279.6		
190120	Tie	515703.25	7552572.13	515703.25	7546778.61	180.0	5.8	4682.8	285.4		
190130	Tie	514327.32	7609956.37	514327.32	7546780.88	180.0	63.2	4682.8	348.6		
190140	Tie	512327.32	7609954.09	512327.32	7546780.88	180.0	63.2	4682.8	411.8		
190150	Tie	510327.32	7609954.09	510327.32	7546780.88	180.0	63.2	4682.8	474.9		
190160	Tie	508612.44	7587782.28	508612.44	7582170.55	180.0	5.6	4682.8	480.6		
190170	Tie	508598.17	7558155.49	508598.17	7548583.14	180.0	9.6	4682.8	490.1		
190180	Tie	508327.32	7582359.76	508327.32	7557983.19	180.0	24.4	4682.8	514.5		
190190	Tie	506875.91	7582359.76	506875.91	7557980.62	180.0	24.4	4682.8	538.9		
190200	Tie	505327.32	7565797.06	505327.32	7561573.07	180.0	4.2	4682.8	543.1		
190210	Tie	505169.80	7582359.75	505169.80	7574561.36	180.0	7.8	4682.8	550.9		
190220	Tie	503449.28	7582359.75	503449.28	7574556.07	180.0	7.8	4682.8	558.7		





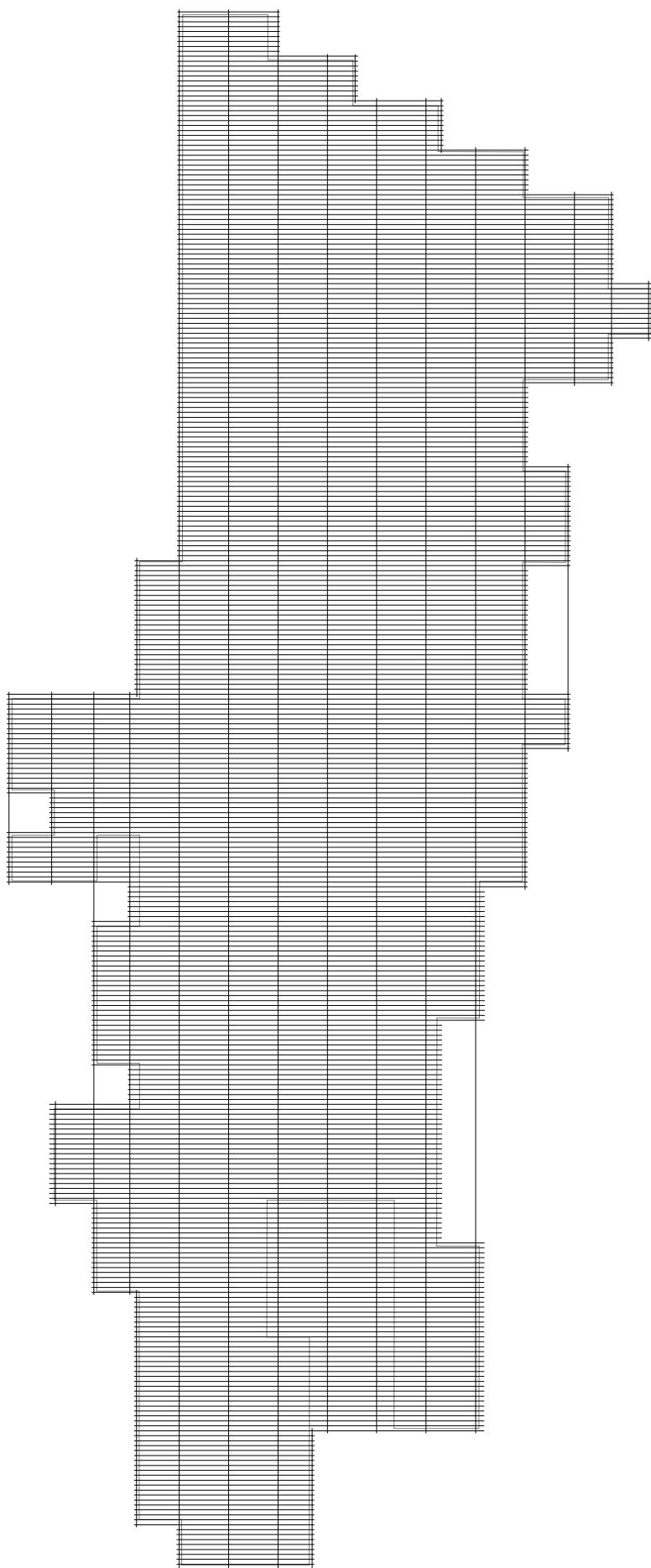


### South Block (Cont)

Line	Type	Easting	Northing	Easting	Northing	Direc	Length	Tv	Cumul	Ti	Cumul
290090	Tie	508522.96	7539935.75	508522.96	7520982.48	180.0	19.0	2206.3	157.2		
290100	Tie	506522.96	7539935.75	506522.96	7520982.48	180.0	19.0	2206.3	176.2		
290110	Tie	505385.26	7543535.87	505385.26	7539748.05	180.0	3.8	2206.3	180.0		
290120	Tie	504522.96	7543534.81	504522.96	7520983.02	180.0	22.6	2206.3	202.5		
290130	Tie	502522.96	7543534.82	502522.96	7520983.02	180.0	22.6	2206.3	225.1		
290140	Tie	501728.58	7543535.37	501728.58	7539774.88	180.0	3.8	2206.3	228.8		
290150	Tie	500522.96	7539936.10	500522.96	7520983.02	180.0	19.0	2206.3	247.8		
290160	Tie	500000.28	7539935.30	500000.28	7520983.73	180.0	19.0	2206.3	266.7		
290170	Tie	503442.91	7534133.84	503442.91	7530558.55	180.0	3.6	2206.3	270.3		

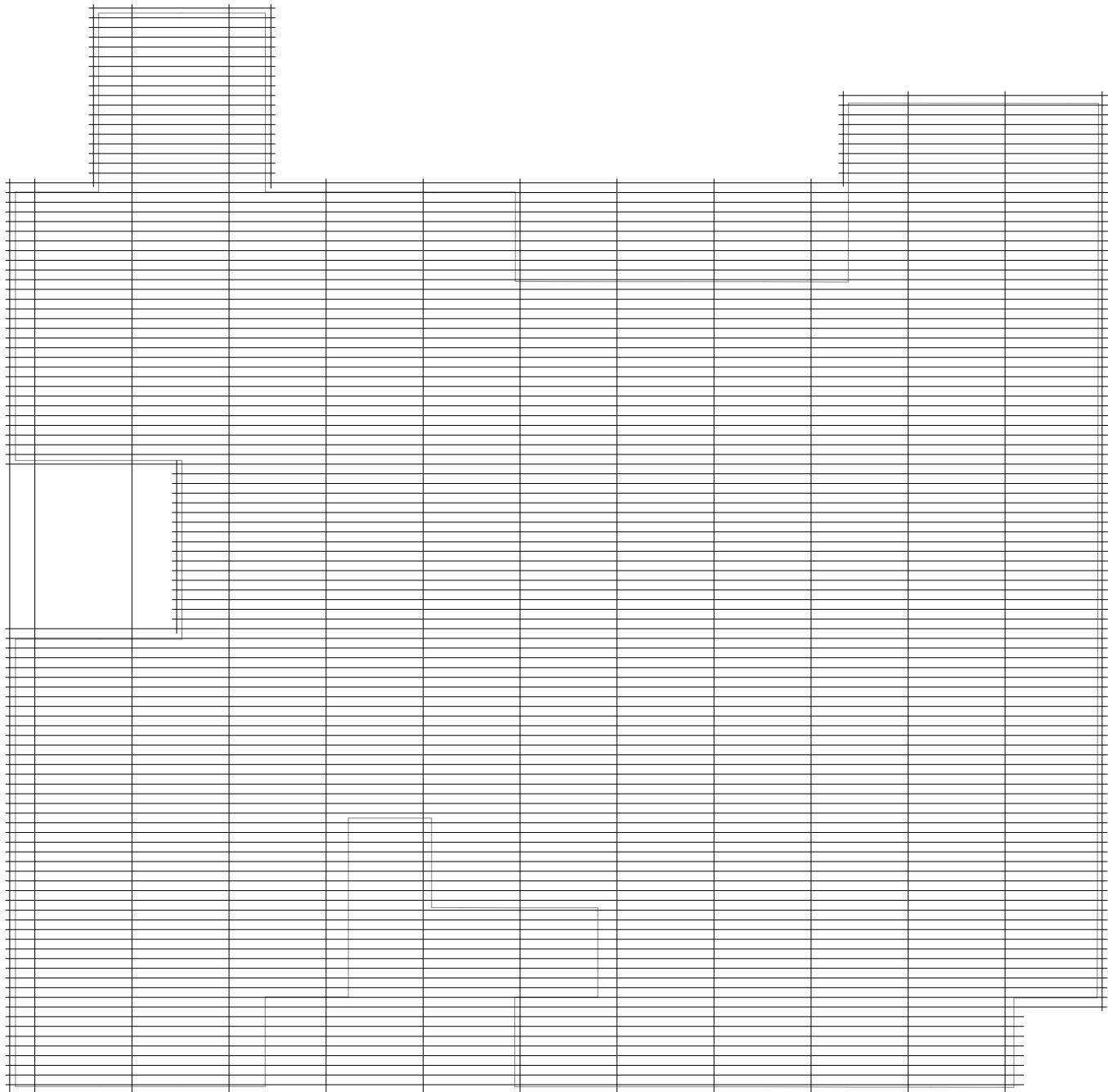


## North Block





## **South Block**



# **HAINES SURVEYS**

**GRAVITY SURVEY SPECIALISTS**



**Job No. 1908**

**ISA B GRAVITY SURVEY**  
**Mawson Resources Ltd.**  
**June 2019**

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## Introduction

A GPS gravity survey designated as Isa B Gravity Survey has been carried out in an area approximately 70 kilometres south of McKinlay in Queensland over 14 days from 17<sup>th</sup> June 2019 to 30<sup>th</sup> June 2019 on behalf of Mawson Resources Ltd.

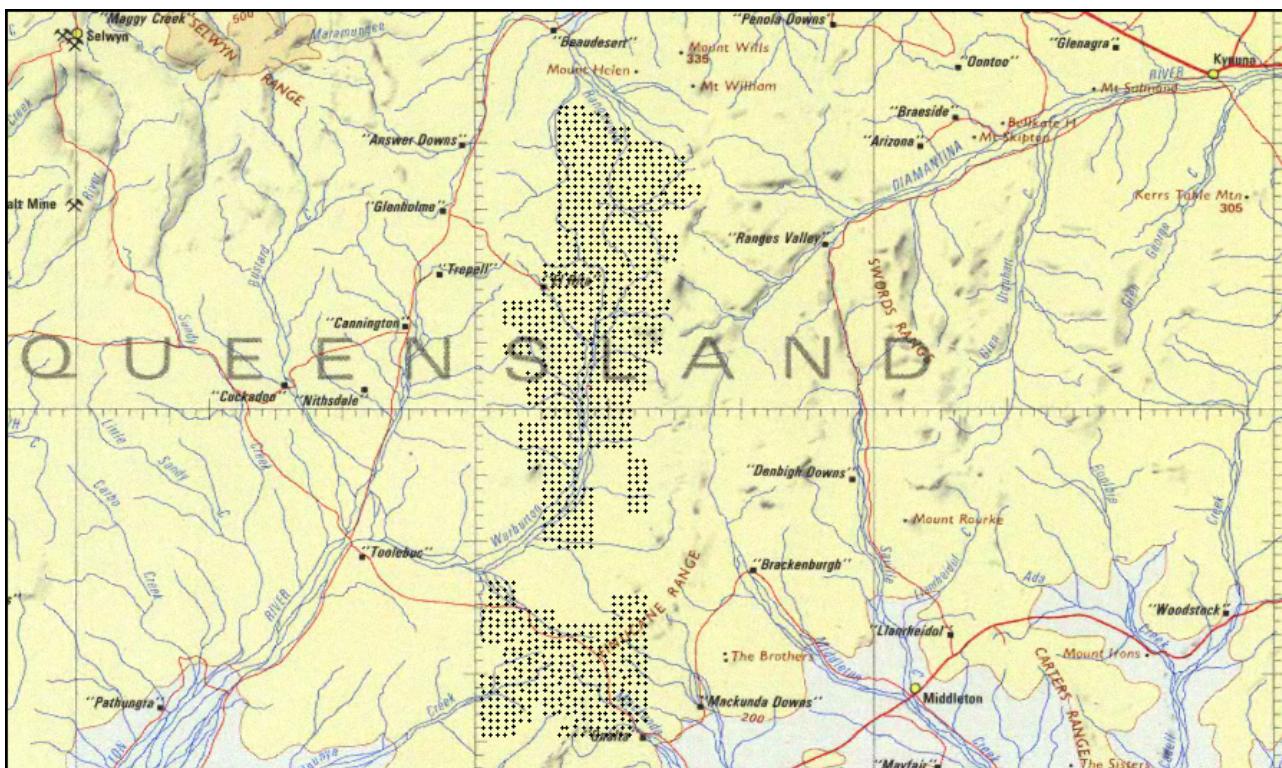
The proposed Isa B Gravity Survey consisted of 1236 gravity stations in an irregular grid comprising 84 West-East trending lines coincident with GDA94 with a line spacing of 1000 metres and station intervals of 1000 metres. The lines of irregular length were bounded in the west by GDA94 Zone 54 501000E, in the east by 529000E, in the south by 7522000N and in the north by 7609000N. The line lengths ranged from 3000 metres to 21000 metres.

The completed Isa B Gravity Survey comprised of 1236 stations in 84 lines. All proposed gravity stations were completed. Note; some of the stations may have been slightly offset from their planned position due to vegetation and terrain.

There were 15 observations repeated for quality control purposes, giving a repeat percentage of 1.2%.

The Bouguer anomaly processing has been performed using a country rock density of 2.67 g/cc.

Figure 1 identifies the location of the survey area.



**Figure 1. General Location Diagram**

## **GPS Survey and Gravity Datum**

Horizontal Datum: Geocentric Datum of Australia1994 (GDA94)  
Map Grid of Australia 1994 (MGA94)  
Zone 54

Vertical Datum: Australian Height Datum (AHD)

Gravity Datum: Australian Absolute Gravity Datum 2007 (AAGD07)

## **Survey and Gravity Base Stations**

Three base stations were established in the survey area. The base locations were selected to ensure all processed GPS baselines were stored within an accurate range, ensuring accurate GPS collection. The bases were designated 2019.0801, 2019.0803 and 2019.0804. The actual bases were marked with a short star picket driven flush with the natural surface. The bases were witnessed by 1m long star pickets within 0.3m of the ground marks. A single aluminium tag is attached to the witnessed post. These tags are inscribed "Haines Surveys" and "Gravity 2019.0801" etc.

## **Survey Control**

Horizontal and vertical control has been established using the AUSPOS online GPS processing service provided by Geoscience Australia. This method provides control within the GDA94 Datum to within +/- 5 cm. It largely replaces the need for finding local survey marks or allows accurate control to be established when local marks are not available.

A total of 92.4 hours (at 5 second intervals) of observations were logged over 7 days. The following outlines the Cartesian coordinate precision attained per day.

1 Sigma	sX(m)	sY(m)	sZ(m)	yyyy/mm/dd
0801	0.008	0.009	0.009	2019/06/17
0801	0.008	0.008	0.009	2019/06/18
0801	0.009	0.009	0.009	2019/06/19
0803	0.011	0.011	0.012	2019/06/18
0803	0.009	0.009	0.010	2019/06/19
0803	0.008	0.009	0.009	2019/06/20
0804	0.010	0.011	0.011	2019/06/23
0804	0.009	0.009	0.010	2019/06/25
0804	0.008	0.009	0.009	2019/06/26

Since GDA94 and WGS84 (Global Positioning System Datum) are virtually equivalent the GDA94 values can be directly input into the GPS processing software for all calculations.

Vertical control has been converted to an Australian Height Datum (AHD) height using the GDA94 height determined from AUSPOS and the AUSGEOD09 gravimetric geoid.

## **Gravity Control**

Gravity control for base station 2019.0801 was established on the Australian Absolute Gravity Datum 2007 (AAGD07) using a series of single one-way ties during mobilisation both to and from Answer Downs Station.

One-way ties were completed to Gravity Stations 2012999054 (Longreach) and 1964911032 (Winton). The values for Gravity Stations 2012999054 (Longreach) and 1964911032 (Winton) were attained from Geoscience Australia in Canberra.

Gravity Control for base stations 2019.0803 and 2019.0804 was established on the Australian Absolute Gravity Datum 2007 (AAGD07) using a series of A-B-B-A ties base station 2019.0801 (Answer Downs Station).

All completed gravity ties ensured that Gravity Control was established to within 0.01 milligals.

## **Survey and Gravity Control Values**

Control information (**WGS84 heights have been derived using AusGeoid09**):

<b>Station</b>	<b>GDA 94</b>			<b>MGA94 Zone 54</b>		<b>AHD</b>	<b>AAGD07</b>	<b>Comments</b>
	<b>Latitude</b>	<b>Longitude</b>	<b>Height</b>	<b>Easting</b>	<b>Northing</b>	<b>Height</b>	<b>Gravity mgal</b>	
2019.0801	-21 40 11.91262	140 59 36.93826	286.792	499337.244	7603701.357	244.077	978688.402	Base 0801
2019.0803	-22 16 49.85012	141 06 45.00269	288.372	511589.451	7536119.237	247.847	978705.410	Base 0803
2019.0804	-21 50 55.10698	141 06 20.24109	313.761	510913.982	7583922.483	271.512	978695.893	Base 0804
2012999054	-23 26 21.696	144 16 16.644	193.00				978776.134	Longreach
1964911032	-22 23 18.510	143 02 16.188	184.74				978730.912	Winton

## **GPS Observations and Processing**

Carrier phase GPS data has been collected using *Trimble R8 GNSS* series geodetic receivers.

Measurements for all post processed observations have been made using Static techniques with baselines processed to double difference fixed solutions resulting in horizontal and vertical precision of approximately 2 cm.

Static baseline and RTK processing has been done using Trimble Business Centre Version 2.50 software.

Details of Horizontal and Vertical control are provided in the section above.

## **Gravity Observations**

Gravity measurements have been made using *Scintrex CG5 Autograv* instruments. Instrument numbers 080440381 and 99080474 were used in this project.

Readings of 120 seconds were taken at all base stations. Readings of 40 seconds were taken at all other gravity survey points.

Base station readings were taken at the beginning, middle and at the end of the day's fieldwork.

All Autograv instruments apply an instrument drift correction to its final gravity reading. Any residual drifts between base station readings are corrected by the gravity post processing software. The instruments also apply Earth Tide Corrections to their final gravity reading at each station. The various instrument calibration constants are contained in the daily gravity data files.

## **Point Numbering and Marking**

An 8 digit point number is used to identify each gravity station. The first 4 digits indicate the line number. The second 4 digits indicate the station number

The lines are West-East and the 8 digits are constructed from the planned GDA coordinates for each gravity station using

$$\text{Line No} = (\text{GDA N} - 7500000) / 10 \quad \text{Stn No} = (\text{GDA E} - 500000) / 10$$

eg. Planned gravity station GDA coordinates

$$7539000.000N \quad 501000.000E$$

$$\text{Line No} = 3900$$

$$\text{Station No} = 0100$$

$$\text{Ie, Pt No} = 3900.0100$$

The gravity stations have not been marked in the field.

## **Gravity Processing**

The gravity values for this survey are related to the *Australian National Gravity Database* using the *Australian Absolute Gravity Datum 2007 (AAGD07)* values at known Gravity Stations as provided by *Geoscience Australia*.

***Note that all gravity values shown in these surveys are expressed in units of milligals.***

The field gravity observations have been processed using standard formulae and constants as documented by *Geoscience Australia* to produce a Bouguer Anomaly for each gravity station.

The meter reading as recorded in the raw Scintrex data file is corrected for instrument tilts, meter drift and Earth Tide. Post processing corrections are detailed below.

Reference:

*V\_GRAV\_JETSTREAM\_AAGD07\_final\_REVISED\_NOV\_2008.pdf*

### **Drift**

The residual drift between base station readings is calculated for each station reading proportionately by time. This is the drift value shown in the processing output.

$$\text{Drift} = \left[ \left( t_n - t_1 \right) \left( (b_2 - b_1) / (t_2 - t_1) \right) \right]$$

$t_n$  = time of meter reading at each station

$b_1$  = base meter reading prior to station reading

$t_1$  = time of base reading  $b_1$

$b_2$  = base meter reading after station reading

$t_2$  = time of base reading  $b_2$

### **Observed Gravity**

This is the observed gravity value in milligals.

$$\text{Obs\_g} = b_g + (r_n - \text{drift}) - b_1$$

$b_g$  = base stn gravity value (AAGD07)

$r_n$  = meter reading at each station as shown in the gravity meter log file

drift = residual drift correction as shown above

$b_1$  = base meter reading prior to station reading

Atmospheric Correction

$$\text{Atmos} = 8.74 - (0.00099 * h) + (0.0000000356 * h^2) / 10$$

$h$  = height above ellipsoid

Anomaly

This is the difference between the observed gravity and the theoretical gravity value at each station. The theoretical value is calculated using the *1980 International Gravity Formula* (Moritz, 1980).

$$g_{\text{th}} = 978032.67715 (1 + 0.001931851353(\sin f))^2 / \sqrt{(1 - 0.0066943800229(\sin f))^2}$$

$f$  = GDA94 Latitude

$$\text{Anom} = \text{Obs}_g - g_{\text{th}} - \text{Atmos}$$

$\text{Obs}$  = observed gravity as explained above

Free Air Correction

The freeair correction is calculated using

$$\text{Freeair} = (3.087691 - 0.004398 \sin^2 f) * h - 7.2125 * 10^{-7} h^2 / 10$$

$h$  = height above ellipsoid

Bouguer Correction

This uses the closed form equation for the gravity effect of a spherical cap of radius 166.7 km based on a spherical Earth with a mean radius of 6,371.0087714 km, height relative to the ellipsoid.

$$\text{Bouguer} = -(2 \pi G r ((1 + \mu) * h - \lambda R)) / 10$$

where

$\pi$  is pi

$G$  is the gravitational constant

=  $6.67428 \times 10^{-11} \text{ m}^3 \text{kg}^{-1} \text{s}^{-2}$  (Mohr and Taylor 2001);

$r$  = density (2.67 g/cc used for this survey)

$h$  is the ellipsoid height in metres of the station

$R$  = ( $R_o + h$ ) the radius of the earth at the station

$R_o$  is the mean radius of the earth = 6,371.0087714 km

GRS 80 value from Moritz or 6,371 km (LaFehr)

$\mu$  &  $\lambda$  are dimensionless coefficients with following definitions

$$\mu = ((1/3) * \eta^2 - \eta)$$

where  $\eta = h/R$

$$\lambda = (1/3) \{ (d + f\delta + \delta^2)[(f - \delta)^2 + k]^{1/2} + p + m * \ln(n/(f - \delta + [(f - \delta)^2 + k]^{1/2})) \}$$

where:

$$d = 3 * \cos^2 \alpha - 2$$

$$f = \cos \alpha$$

$$k = \sin^2 \alpha$$

$$p = -6 * \cos^2 \alpha \sin(\alpha/2) + 4 * \sin^3(\alpha/2)$$

$$\delta = R_o/R$$

$$m = -3 * \sin^2 \alpha \cos \alpha = -3 * k * f$$

$$n = 2 * [\sin(\alpha/2) - \sin^2(\alpha/2)]$$

$$\alpha = S/R_0$$

$$S = \text{Bullard B Surface radius} = 166.735 \text{ km.}$$

Bouguer Anomaly

Bouguer Anomaly = Anomaly + Freeair + Bouguer

Geoidal Bouguer Anomaly

Free Air Anomalies and Bouguer Anomalies are also provided using geoid heights and an infinite slab Bouguer correction. They are designated as Geoidal Free Air Anomaly and Geoidal Bouguer Anomaly respectively.

These anomalies are calculated with the formulae in use prior to 5 February 2008 when the AAGD07 gravity datum was implemented. These formulae are:

Theoretical gravity based on the 1967 international gravity formula:

$$G_{th} = 978031.8456 * (1 + 0.005278895 \sin^2\phi + 0.000023462 \sin^4\phi)$$

$$\text{Geoidal FreeAir} = ((3.08768 - 0.00440 \sin^2\phi) * H - 0.000001442 * H^2) / 10$$

$$G_{FreeAirAnom} = \text{Obs}_g - G_{th} + \text{Geoidal FreeAir}$$

$$\text{Geoidal Bouguer} = -0.04191 * H * r$$

f = GDA94 Latitude

H = Geoid Height (ground elevation)

r = density (2.67 g/cc used for this survey )

$$\text{Geoidal Bouguer Anomaly} = G_{Obs} - G_{th} + \text{Geoidal FreeAir} + \text{Geoidal Bouguer}$$

**NOTE:** The Geoidal Free Air and Geoidal Bouguer Anomalies calculated using geoid heights and the infinite slab model will NOT be the same as those obtained prior to 5 February 2008. The data are now referenced to the new gravity datum AAGD07. Data prior to 5 February 2008 were in the ISOGAL84 gravity datum.

To convert observed gravity values from ISOGAL84 to AAGD07, the following formula can be used:

$$g(\text{AAGD07}) = g(\text{ISOGAL84}) - 0.078 \text{ mGal}$$

## Results Formats

### CSV Format

This is a Comma Separated Variable format file. This format facilitates data import into spreadsheet and database software. Each record (line) contains the following data fields:

"Pt#"	Station identifiers used in data loggers, line and station numbers combined
"Line"	Station line number
"Stn"	Station number
"Date"	Date of observation
"Day"	GPS day number
"Time"	Time of observation
"GDA94_Lat"	WGS84/GDA94 Latitude used in GPS observation
"GDA94_Long"	WGS84/GDA94 Longitude used in GPS observation
"GDA94_Ht"	Height above the ellipsoid defined by the WGS84 Datum
"MGA94(ZONE54)E"	Easting value for observation on the MGA94/GDA94 Datum
"MGA94(ZONE54)N"	Northing value for observation on the MGA94/GDA94 Datum
"AHD_Ht"	Height of observation in the Australian Height Datum
"Meter_Ser_No"	Gravity meter serial number
"Meter_Rdg"	Gravity meter observation value in mGals
"Meter_Error"	Measurement of the quality of the gravity observation (a function of the SD of the observation set used and the duration of the set)
"ETC"	Earth Tide Correction applied to the gravity observation
"Drift"	The component of the meter drift between opening and closing gravity base observations applied to the observation
"Corr_Meter"	The meter observation with the drift applied
"dg"	The difference in gravity between the base and the observation
"Obs_g"	Observed gravity of the station
"Anom"	Difference between observed and theoretical gravity minus atmospheric corn.
"Freeair"	Free air correction (see above)
"Bouguer(2.67)"	Bouguer correction using a density of 2.67g/cc (see above)
"Bouguer_Anom"	Bouguer anomaly (see above)
"Geoid_Anom"	Difference between observed and theoretical gravity
"Geoid_Freeair"	Geoid Free air correction (see above)
"Geoid_Bouguer"	Geoid Bouguer correction using a density of 2.67g/cc (see above)
"Geoid_Bouguer_Anom"	Geoid Bouguer anomaly (see above)

## Production Log

Date	Day#	Obs	Repeats	Crews	Comments
17/06/2019	168	96	0	1	Bases 2019.0801 and 2019.0802 established
18/06/2019	169	100	2	1	Base 2019.0803 established
19/06/2019	170	106	2	1	
20/06/2019	171	91	1	1	
21/06/2019	172	94	1	1	
22/06/2019	173	92	1	1	
23/06/2019	174	103	1	1	Base 2019.0804 established
24/06/2019	175	0	0	1	Standby, Scheduled Helicopter Service
25/06/2019	176	102	1	1	
26/06/2019	177	105	1	1	
27/06/2019	178	104	1	1	
28/06/2019	179	101	1	1	
29/06/2019	180	98	1	1	
30/06/2019	181	44	2	1	Survey completed
	<b>Total</b>	<b>1236</b>	<b>15</b>		

## Repeat Observation Results

### ISA B GRAVITY SURVEY

Pt #	Day	E	N	H	G	Bouguer
1001500	D168	514,948.401	7,600,959.156	256.644	978,686.854	+7.536
1001500	D169	514,948.397 +0.004	7,600,959.148 +0.008	256.681 -0.037	978,686.847 +0.007	+7.536 +0.000
1001600	D168	516,003.848	7,600,963.376	249.902	978,688.539	+7.906
1001600	D181	516,003.897 -0.049	7,600,963.332 +0.044	249.916 -0.014	978,688.513 +0.026	+7.883 +0.023
4001100	D168	511,018.611	7,604,026.700	235.109	978,690.547	+8.751
4001100	D169	511,018.478 +0.133	7,604,026.675 +0.025	235.103 +0.006	978,690.577 -0.030	+8.780 -0.029
36002200	D169	521,953.597	7,536,003.700	245.701	978,718.093	-0.511
36002200	D170	521,953.832 -0.235	7,536,003.554 +0.146	245.699 +0.002	978,718.089 +0.004	-0.515 +0.004
37001200	D169	512,018.203	7,536,990.209	245.538	978,706.592	-11.504
37001200	D170	512,018.178 +0.025	7,536,990.222 -0.013	245.536 +0.002	978,706.571 +0.021	-11.526 +0.022
30000800	D170	508,043.589	7,529,979.740	241.851	978,713.025	-9.854
30000800	D171	508,043.596 -0.007	7,529,979.750 -0.010	241.855 -0.004	978,713.046 -0.021	-9.832 -0.022
26001200	D171	512,002.253	7,525,941.635	271.663	978,710.780	-8.611
26001200	D172	512,002.257 -0.004	7,525,941.643 -0.008	271.652 +0.011	978,710.792 -0.012	-8.601 -0.010
50001200	D172	511,995.518	7,549,976.788	234.098	978,712.151	-0.672
50001200	D173	511,995.487 +0.031	7,549,976.798 -0.010	234.078 +0.020	978,712.143 +0.008	-0.684 +0.012

60000900	D173	508,989.861	7,560,003.282	246.548	978,709.023	+4.401
60000900	D174	508,989.861	7,560,003.323	246.551	978,709.014	+4.393
		+0.000	-0.041	-0.003	+0.009	+0.008
68001100	D174	511,000.548	7,567,998.719	252.772	978,708.817	+10.008
68001100	D176	511,000.531	7,567,998.699	252.783	978,708.770	+9.963
		+0.017	+0.020	-0.011	+0.047	+0.045
75001200	D176	512,004.027	7,575,009.139	260.569	978,703.760	+10.487
75001200	D177	512,004.037	7,575,009.153	260.552	978,703.773	+10.498
		-0.010	-0.014	+0.017	-0.013	-0.011
80001100	D177	511,017.547	7,580,000.985	262.620	978,701.034	+11.007
80001100	D178	511,017.538	7,580,001.002	262.621	978,701.001	+10.974
		+0.009	-0.017	-0.001	+0.033	+0.033
86002000	D178	520,020.998	7,585,985.132	304.766	978,686.008	+7.625
86002000	D179	520,021.030	7,585,985.153	304.790	978,685.966	+7.587
		-0.032	-0.021	-0.024	+0.042	+0.038
92001500	D179	514,994.611	7,592,016.152	274.287	978,687.188	+6.263
92001500	D180	514,994.591	7,592,016.144	274.281	978,687.236	+6.310
		+0.020	+0.008	+0.006	-0.048	-0.047
98001700	D180	517,005.890	7,597,950.799	241.863	978,690.073	+6.169
98001700	D181	517,005.897	7,597,950.823	241.853	978,690.062	+6.156
		-0.007	-0.024	+0.010	+0.011	+0.013

### **Bouguer – Elevation Profiles**

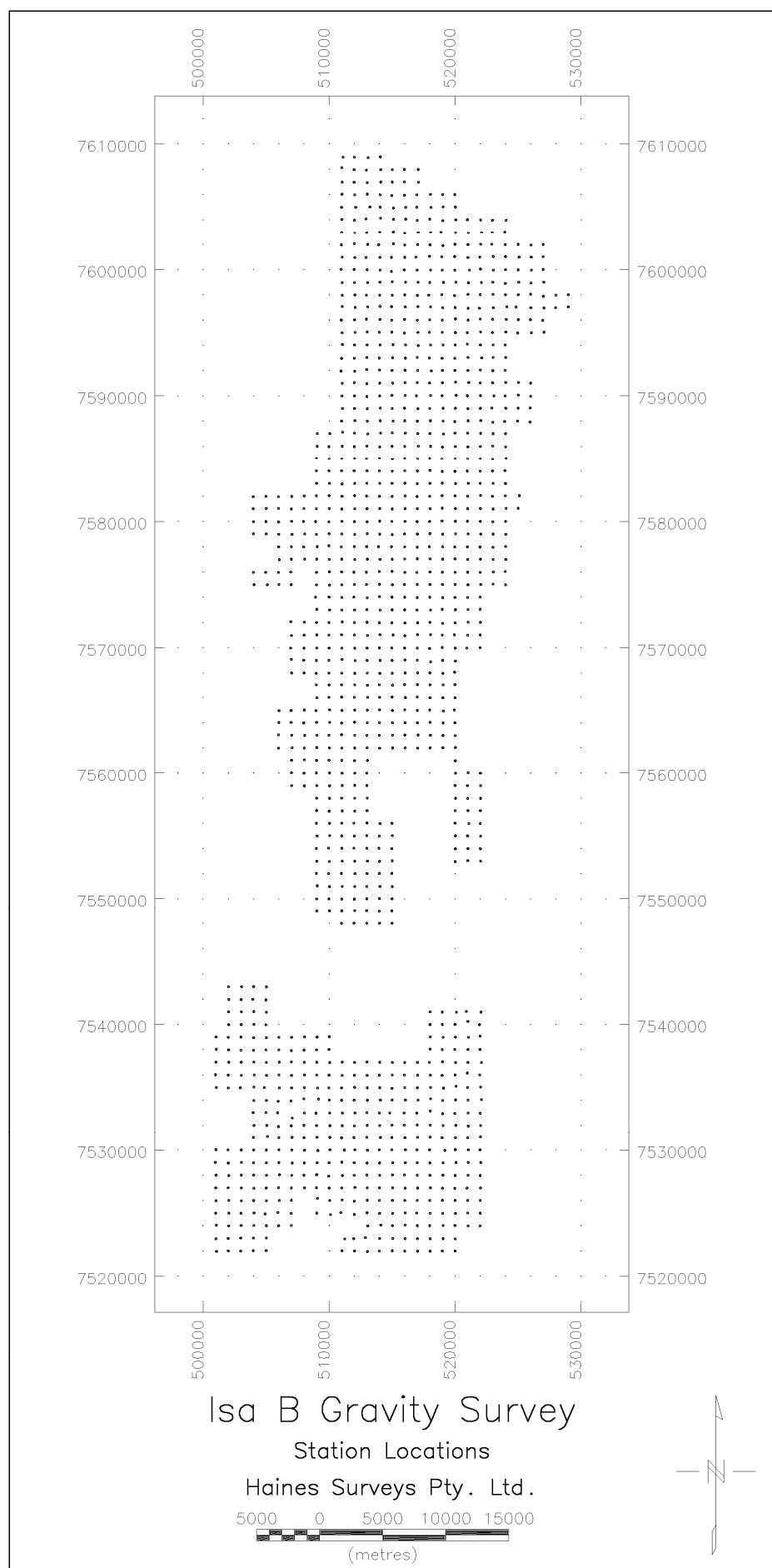
Please refer to the folder titled 'Bouguer – Elevation Profiles' on the accompanying CD for bit map images of all the lines completed throughout the project.

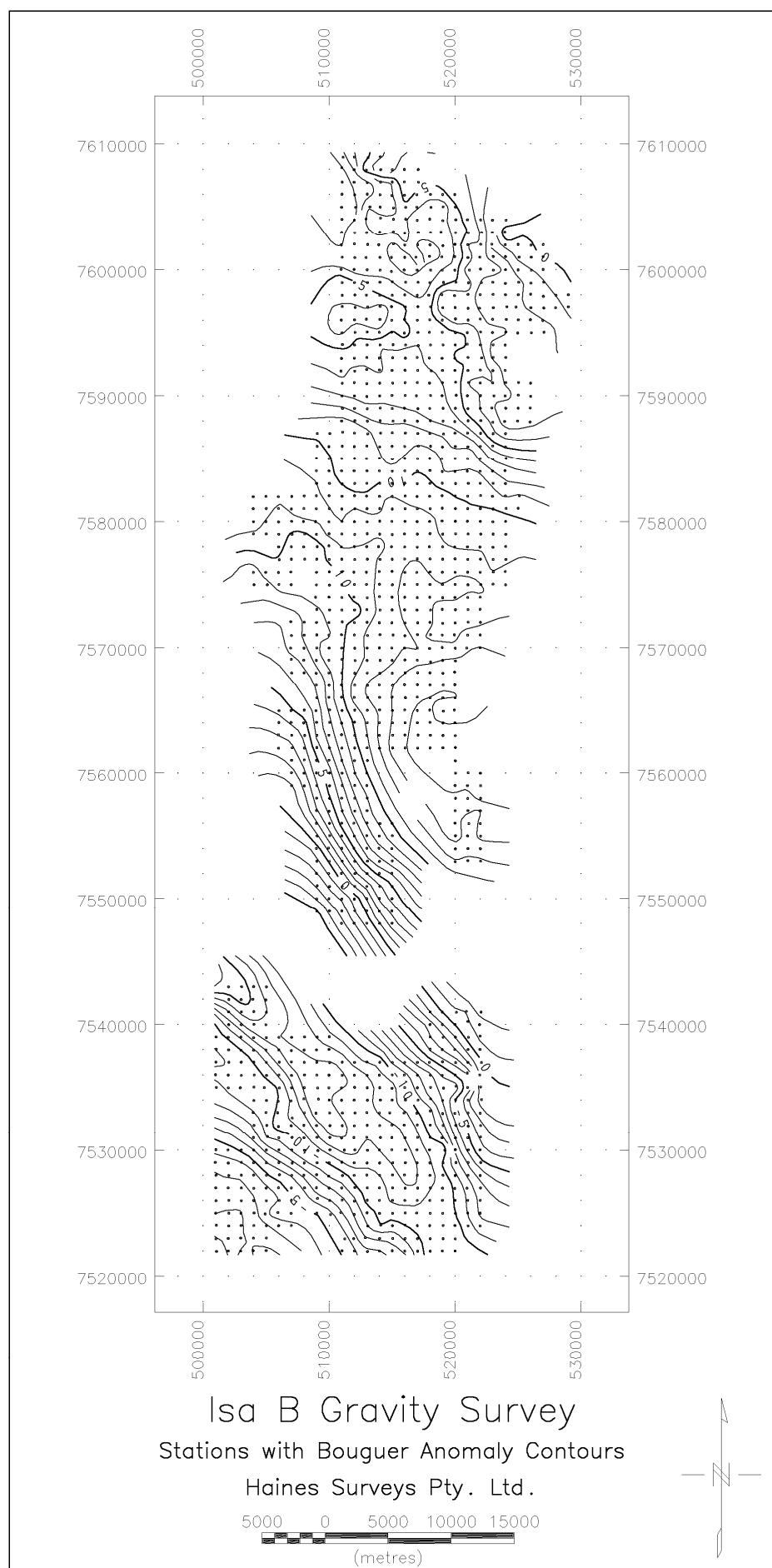
Isa B Gravity Survey, Bouguer – Elevation Profiles available for the following lines:

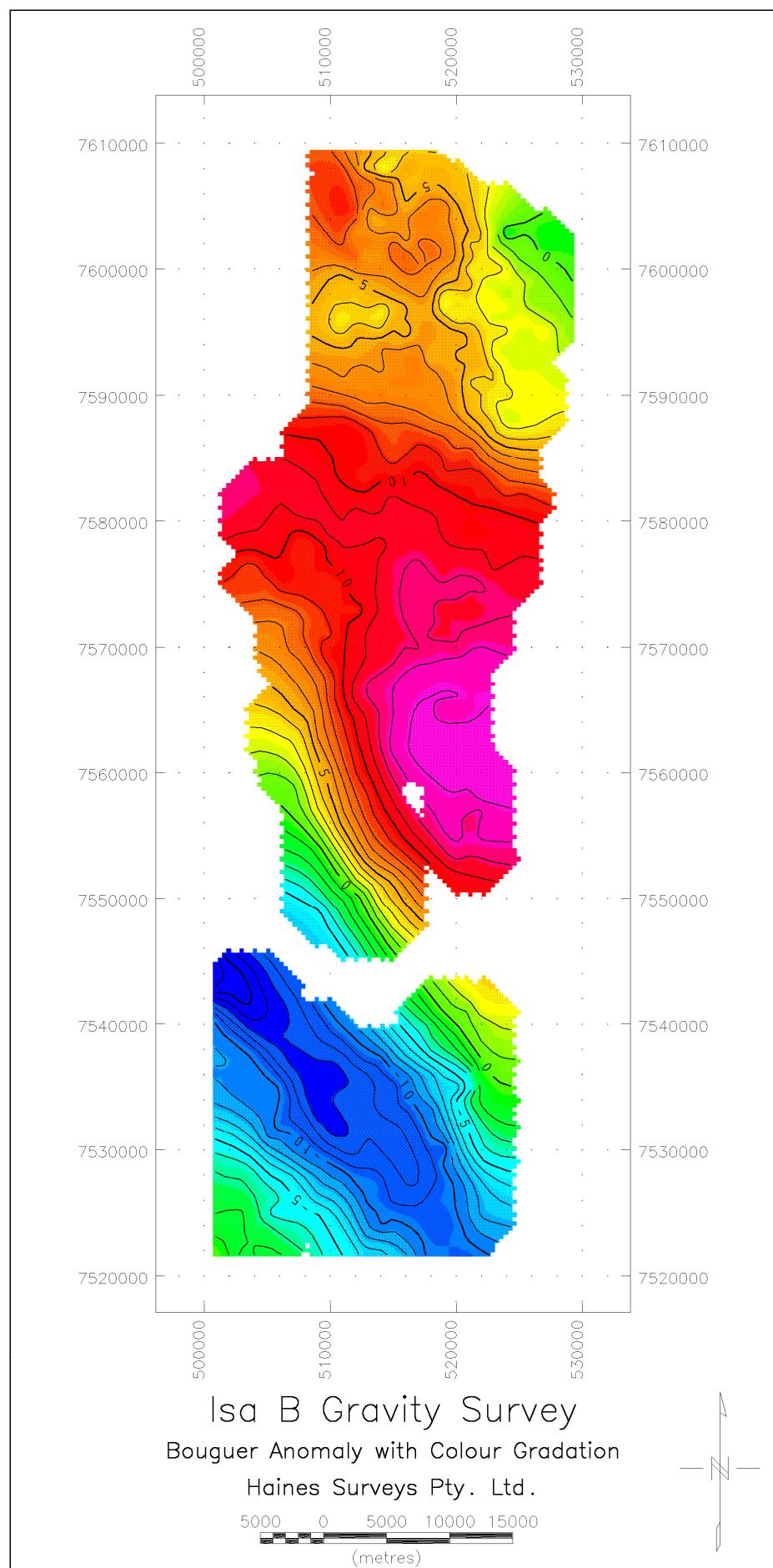
Line	Line	Line	Line	Line
2200	3900	6000	7700	9400
2300	4000	6100	7800	9500
2400	4100	6200	7900	9600
2500	4200	6300	8000	9700
2600	4300	6400	8100	9800
2700	4800	6500	8200	9900
2800	4900	6600	8300	0
2900	5000	6700	8400	100
3000	5100	6800	8500	200
3100	5200	6900	8600	300
3200	5300	7000	8700	400
3300	5400	7100	8800	500
3400	5500	7200	8900	600
3500	5600	7300	9000	700
3600	5700	7400	9100	800
3700	5800	7500	9200	900
3800	5900	7600	9300	

**Plots**

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## PROCESSED RESULTS

### ISA B GRAVITY SURVEY

/	COORDS	GRID	drift	corr'd	obs	anom	freeair	bouguer	bouguer	height
/	E	N	x	y	meter	mgal	corr	corr	anom	(AHD)
/										( 2.67)
/D168										
/ 499337.2	7603701.4	0	801	+0.000	5300.189	978688.402	-47.853	88.529	-32.503	8.174 244.077
/ 499337.2	7603701.4	0	801	+0.000	5300.189	978688.402	-47.853	88.529	-32.503	8.174 244.077
/ 499337.2	7603701.4	0	801	-0.026	5300.189	978688.402	-47.853	88.529	-32.503	8.174 244.077
/ 499337.2	7603701.4	0	801	+0.000	5300.215	978688.402	-47.853	88.529	-32.503	8.174 244.077
514948.4	7600959.2	100	1500	-0.025	5298.641	978686.854	-50.933	92.386	-33.918	7.536 256.644
516003.8	7600963.4	100	1600	-0.024	5300.326	978688.539	-49.244	90.304	-33.154	7.906 249.902
516895.9	7600978.6	100	1700	-0.024	5295.798	978684.011	-53.765	95.140	-34.928	6.448 265.572
517965.6	7601045.9	100	1800	-0.024	5302.600	978690.813	-46.921	85.759	-31.487	7.352 235.186
518945.2	7601009.7	100	1900	-0.024	5301.347	978689.560	-48.194	87.173	-32.005	6.974 239.771
519964.3	7601027.8	100	2000	-0.024	5300.195	978688.408	-49.336	87.412	-32.093	5.984 240.548
521016.2	7600951.2	100	2100	-0.024	5296.825	978685.038	-52.749	91.018	-33.415	4.853 252.233
521968.9	7600982.1	100	2200	-0.023	5285.417	978673.630	-64.144	106.098	-38.946	3.008 301.093
523030.5	7601034.3	100	2300	-0.023	5284.323	978672.536	-65.208	107.241	-39.366	2.667 304.801
523998.1	7601024.2	100	2400	-0.023	5284.107	978672.320	-65.429	106.240	-38.999	1.813 301.562
525083.5	7600987.7	100	2500	-0.023	5281.631	978669.844	-67.925	108.407	-39.793	0.689 308.590
526043.9	7600980.2	100	2600	-0.023	5287.540	978675.753	-62.016	99.025	-36.353	0.656 278.199
526983.7	7601020.4	100	2700	-0.023	5286.868	978675.081	-62.665	99.044	-36.359	0.020 278.265
510977.1	7601955.2	200	1100	-0.019	5302.521	978690.734	-46.495	86.214	-31.653	8.066 236.623
512006.3	7602044.7	200	1200	-0.020	5292.442	978680.655	-56.528	100.280	-36.813	6.939 282.191
513059.5	7601985.6	200	1300	-0.020	5294.183	978682.396	-54.819	97.712	-35.871	7.023 273.875
513936.1	7601962.6	200	1400	-0.020	5288.725	978676.938	-60.291	105.184	-38.611	6.281 298.081
515101.1	7602042.6	200	1500	-0.020	5297.193	978685.406	-51.774	93.684	-34.394	7.516 260.827
516000.1	7601948.4	200	1600	-0.021	5287.636	978675.849	-61.388	106.342	-39.036	5.919 301.842
517028.9	7601964.9	200	1700	-0.021	5299.270	978687.483	-49.739	89.933	-33.018	7.177 248.686
518010.7	7601954.1	200	1800	-0.021	5301.728	978689.941	-47.285	86.112	-31.616	7.211 236.310
519030.8	7601892.3	200	1900	-0.021	5301.942	978690.155	-47.105	85.095	-31.243	6.748 233.023
519991.5	7601996.2	200	2000	-0.021	5300.005	978688.218	-48.983	86.578	-31.787	5.808 237.828
521018.9	7601971.4	200	2100	-0.021	5290.762	978678.975	-58.243	97.880	-35.933	3.705 274.448
522035.6	7601998.1	200	2200	-0.022	5295.003	978683.216	-53.984	91.704	-33.667	4.052 254.442
522912.1	7602014.0	200	2300	-0.022	5283.094	978671.307	-65.888	106.720	-39.174	1.657 303.094
523984.1	7601971.8	200	2400	-0.022	5281.163	978669.376	-67.843	108.383	-39.785	0.756 308.492
525004.7	7601989.9	200	2500	-0.022	5288.298	978676.511	-60.693	97.462	-35.779	0.990 273.115
526023.8	7601943.4	200	2600	-0.022	5288.909	978677.122	-60.107	95.453	-35.042	0.304 266.612
526997.2	7601985.7	200	2700	-0.022	5286.324	978674.537	-62.668	97.392	-35.754	-1.029 272.900
510996.2	7602975.9	300	1100	-0.019	5301.757	978689.970	-46.688	86.979	-31.934	8.357 239.079
512032.4	7602937.4	300	1200	-0.019	5288.903	978677.116	-59.568	104.303	-38.288	6.446 295.206
512980.3	7602955.7	300	1300	-0.019	5287.552	978675.765	-60.909	106.265	-39.008	6.348 301.562
514015.4	7602990.0	300	1400	-0.019	5286.234	978674.447	-62.208	107.404	-39.425	5.770 305.253
515098.0	7603021.5	300	1500	-0.018	5285.786	978673.999	-62.638	108.316	-39.760	5.918 308.212
516011.1	7602916.1	300	1600	-0.018	5286.355	978674.568	-62.127	107.050	-39.296	5.627 304.116
517076.4	7602969.3	300	1700	-0.018	5298.381	978686.594	-50.065	89.652	-32.914	6.672 247.754
518051.0	7602969.4	300	1800	-0.018	5300.235	978688.448	-48.210	86.474	-31.749	6.515 237.463
518879.8	7603005.0	300	1900	-0.018	5301.566	978689.779	-46.858	84.404	-30.989	6.557 230.763
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513992.3	7526011.2	2600	1400	+0.004	5330.901	978716.254	-64.019	84.757	-31.119	-10.382	234.371
515027.3	7526007.5	2600	1500	+0.005	5331.627	978716.980	-63.294	82.214	-30.186	-11.267	226.134
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516992.9	7525998.7	2600	1700	+0.006	5332.785	978718.138	-62.139	80.381	-29.514	-11.272	220.197
517995.0	7526005.7	2600	1800	+0.006	5334.077	978719.430	-60.842	79.317	-29.124	-10.649	216.746
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521007.0	7526002.5	2600	2100	+0.008	5335.228	978720.581	-59.691	80.276	-29.475	-8.891	219.829
521999.6	7526007.8	2600	2200	+0.009	5335.547	978720.900	-59.369	81.503	-29.925	-7.791	223.795
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510027.7	7548985.9	4900	1000	+0.054	5324.730	978710.117	-57.023	84.185	-30.909	-3.748	231.731
511005.6	7548982.1	4900	1100	+0.053	5325.714	978711.101	-56.041	84.465	-31.012	-2.588	232.623
512038.6	7549007.0	4900	1200	+0.052	5327.100	978712.487	-54.641	84.824	-31.144	-0.961	233.766
512980.0	7549000.2	4900	1300	+0.051	5327.937	978713.324	-53.807	85.471	-31.381	0.283	235.846
513984.0	7548960.8	4900	1400	+0.050	5329.355	978714.742	-52.411	85.958	-31.560	1.987	237.405
514979.8	7548984.7	4900	1500	+0.049	5330.246	978715.633	-51.506	86.537	-31.772	3.258	239.261
509012.4	7549997.7	5000	900	+0.056	5324.237	978709.624	-56.940	83.942	-30.820	-3.819	230.921
509990.8	7550001.2	5000	1000	+0.057	5325.346	978710.733	-55.829	84.057	-30.862	-2.634	231.277
511006.2	7549979.3	5000	1100	+0.058	5325.751	978711.138	-55.436	84.560	-31.047	-1.923	232.890
511995.5	7549976.8	5000	1200	+0.059	5326.764	978712.151	-54.424	84.938	-31.186	-0.672	234.098
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509051.1	7551032.8	5100	900	-0.015	5325.458	978710.170	-55.805	83.630	-30.706	-2.881	229.869
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512989.1	7550982.9	5100	1300	-0.012	5329.775	978714.487	-51.515	85.234	-31.294	2.425	234.995
514033.2	7550986.8	5100	1400	-0.011	5330.800	978715.512	-50.488	85.813	-31.507	3.819	236.851
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